

Geophysical and Mineralogical Controls on the Rheology of Fracture Slip and Seal Breaching

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U.S. Department of Energy
National Energy Technology Laboratory
Mastering the Subsurface Through Technology, Innovation and Collaboration:
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Presentation Outline

- Benefits
- Project Overview
- Technical Status
 - Premise
 - Observations and Active Experimentation
 - Meso-Scale Observations
 - Appropriate Caprocks
 - Velocity-Stepping Experiments – permeability and stability
 - Slide-Hold-Slide Experiments – permeability and recurrence
 - Micro-Scale Observations
 - Sintering
 - xCT Imaging
 - Analysis at Micro-Scale
 - Digital Rock Physics (DRP) models – permeability and stability
 - Continuum – permeability and stiffness
- Accomplishments
- Synergistic Opportunities
- Summary

Benefit to the Program

Addresses:

Area of Interest 1, Geomechanical Research

.....to determine the constraints of whether seals transected by blind faults will fail seismically or aseismically when contacted by increased reservoir pressures including CO₂ and the implications of this rupture on seal breaching and loss of inventory.

Relevance to FOA (“*in italics*”)

This project will provide:

“improved understanding of geomechanical processes and impacts critical to scCO₂ injection operations.

This [project specifically] includes [and integrates]: theoretical studies, [and] laboratory, work to:

(a) evaluate and assess the probability of induced seismicity;

(b) understand, characterize, and measure potential permeability changes from slip along existing faults; and

(c) understand and assess the geomechanical behavior and effects of increased reservoir pressure on fractures, faults, and sealing formations.”

This will include.....

Project Overview: Goals and Objectives

Examine geophysical and mineralogical controls of caprocks on:

- **Fault slip** – Stable/unstable or aseismic/seismic
- **Permeability evolution** – Sense and magnitude
- **Potential for seal breaching** – Permeability and capillary behavior

Including:

- *Nature, form and **rates of weakening*** that condition whether fractures and faults fail either **seismically** or **aseismically**
- *Nature, form and **rates of healing*** that define whether fractures may strengthen and then re-fail on multiple successive occasions, and
- **Permeability evolution** (*enhancement or destruction*) that is driven on fractures as a consequence of these behaviors
- Feedbacks on healing conditioned both by *physical and chemical transformations* and the redistribution of mineral mass driven by fluid transport.

Technical Status & Methodology

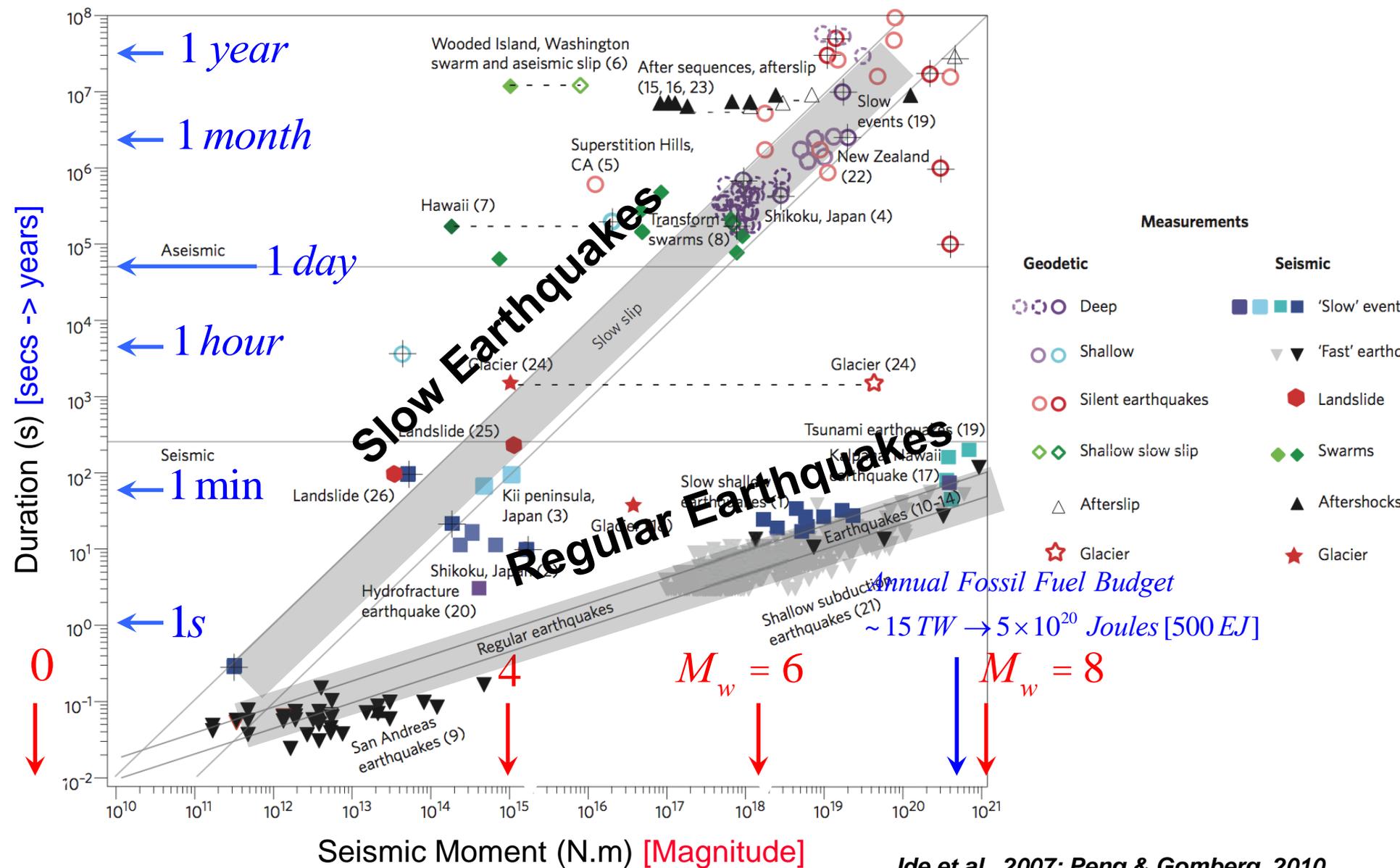
Background

- Felt seismicity
 - Stable versus unstable slip
 - Mineralogical controls
 - Geometric (stiffness) controls
- Seal breaching
 - Evolution of permeability and capillarity characteristics

Methodology

- **Collect, Synthesize and Characterize Sedimentary Formation Samples (Fitts, Lead)**
 - Collect Homogeneous and Mineralogically Complex Sedimentary Rocks (Peters)
 - Sinter Mineral Mixtures to Create Idealized Analogs of Sedimentary Rocks (Fitts)
 - Conduct Baseline Characterization of Natural and Synthetic Caprocks (Fitts)
- **Laboratory Experimentation (Elsworth, Lead)**
 - Evolution of Fault Rheology and Transport Parameters (Elsworth)
 - 3D Imaging of fault contact area, fault geometry, and mineralogy & textures (Fitts)
- **Modeling for Response and for Caprock Screening (Elsworth, Lead)**
 - Digital Rock Physics Modeling of Response (Elsworth)
 - Caprock Screening Heuristics (Peters, Fitts)

Subduction Zone Megathrusts and the Full Spectrum of Fault Slip Behavior



Requirements for Instability

1. Shear strength on the fault is exceeded
- *i.e.*

$$\tau > \mu \sigma'_n$$

2. When failure occurs, strength is velocity (or strain) weakening - *i.e.*

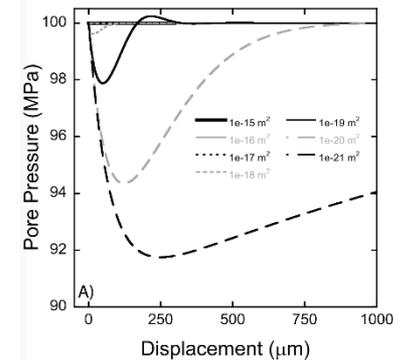
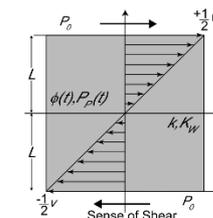
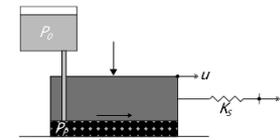
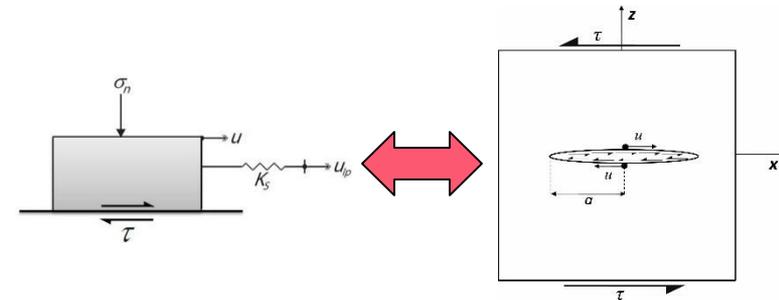
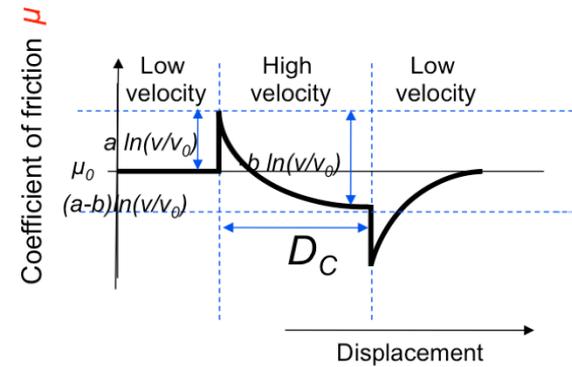
$$a - b < 0$$

2. That the failure is capable of ejecting the stored strain energy adjacent to the fault (shear modulus and fault length) - *i.e.*

$$\frac{G}{l} < K_c = \frac{(b-a)\sigma'_n}{D_c}$$

4. That effective normal stresses evolve that do not dilatantly harden the fault and arrest it via the failure criterion of #1 - *i.e.*

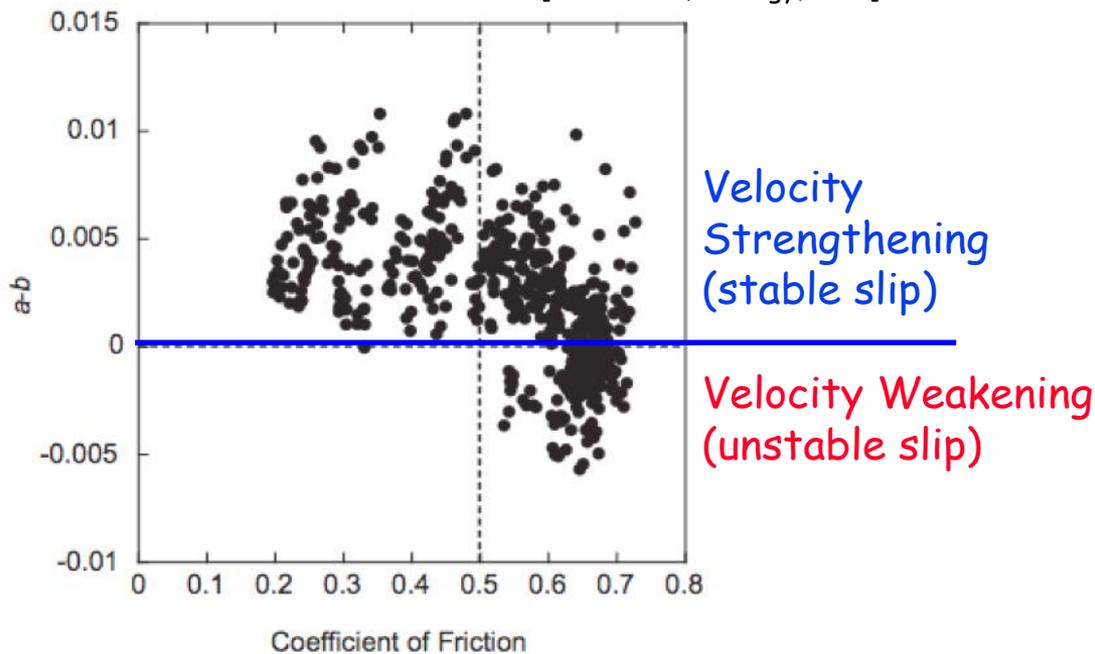
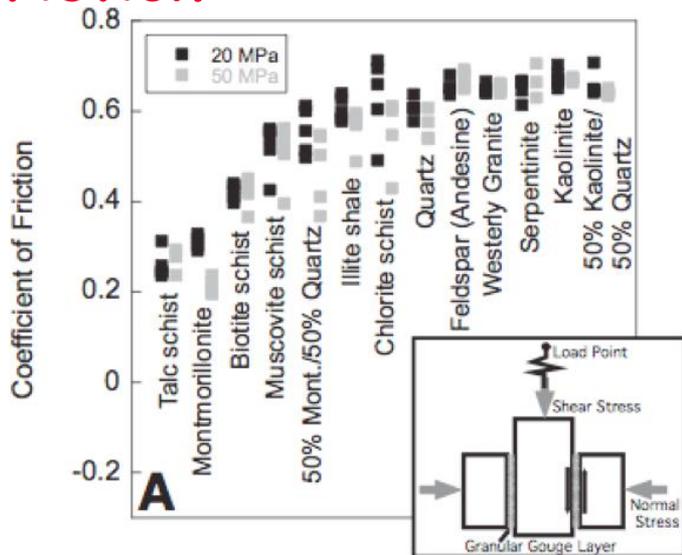
$$1 \gg v_D = \frac{w^2}{k} \frac{v_s \eta}{K_s D_c}$$



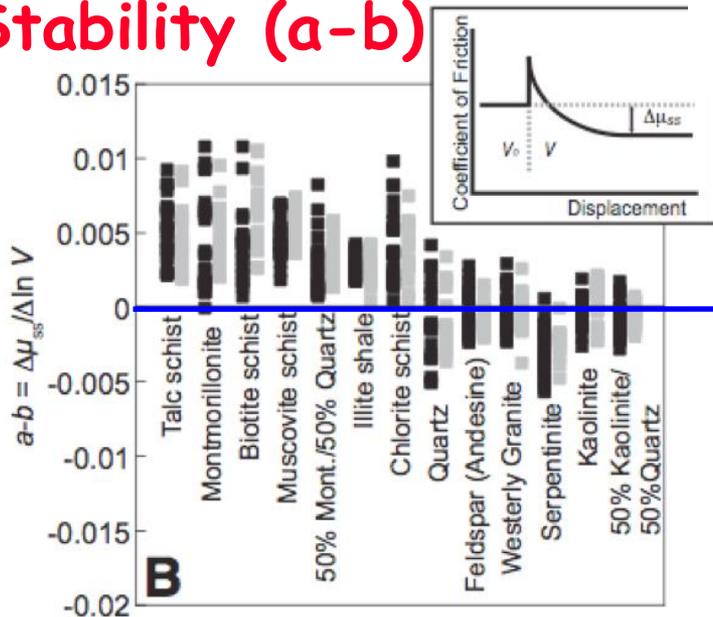
Mineralogical Controls on Instability

Friction

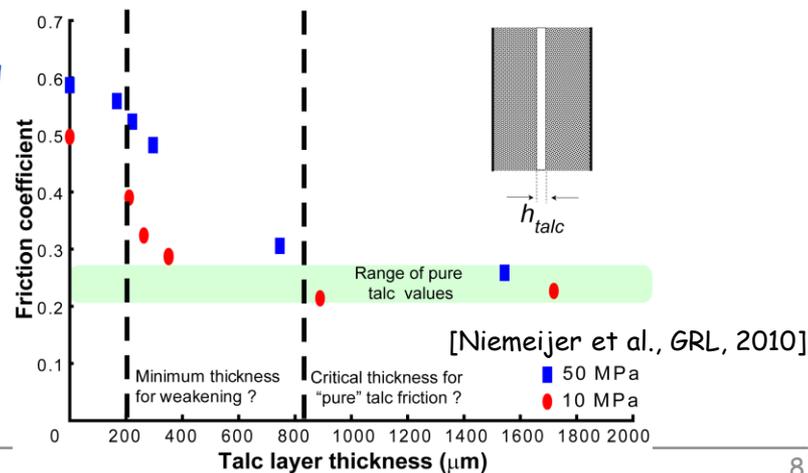
[Ikari et al., *Geology*, 2011]



Stability (a-b)



Frictional Response of Mixtures



[Niemeijer et al., *GRL*, 2010]

Aseismic-Seismic Transition



Scale Dependence - the need for URLs and constrained experimentation at meso scale.

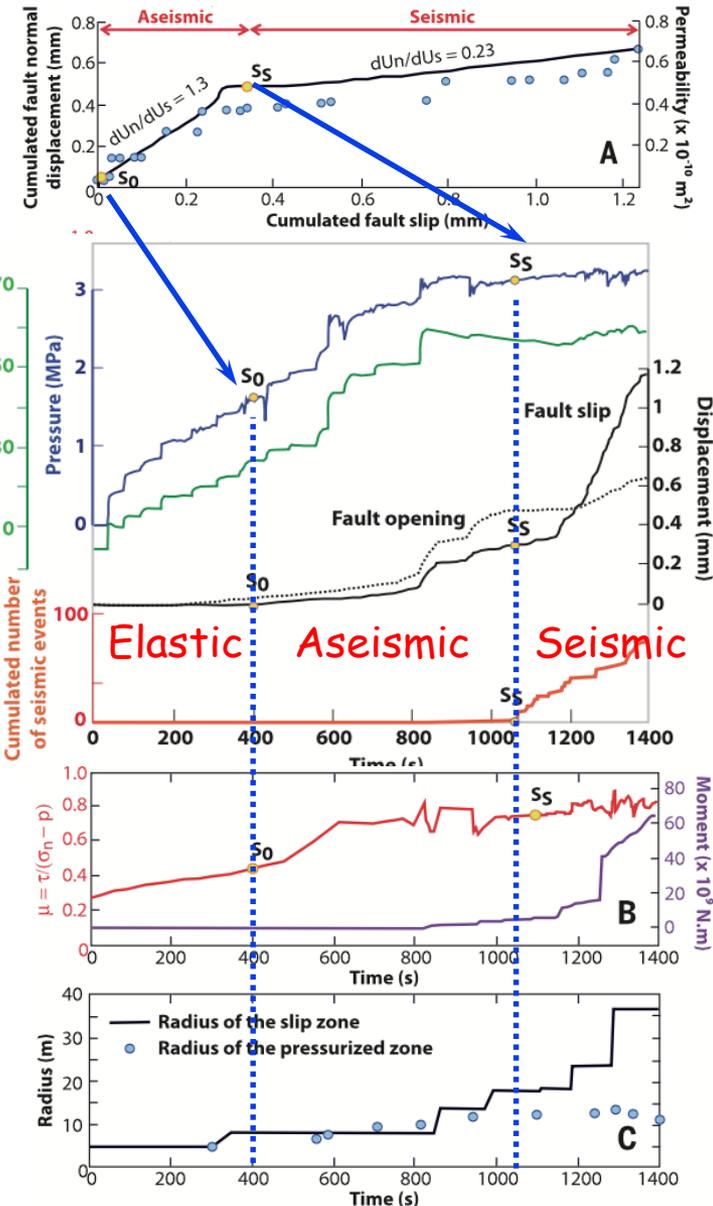
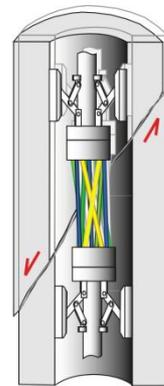
Roles of:

Pressurization ($\sigma_n \rightarrow 0$)

Deformation ahead of the fluid front

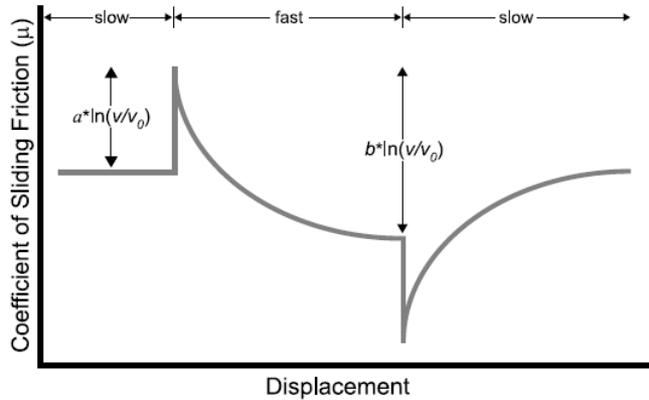
Mineralogical controls

[Guglielmi et al., Science, 2015]

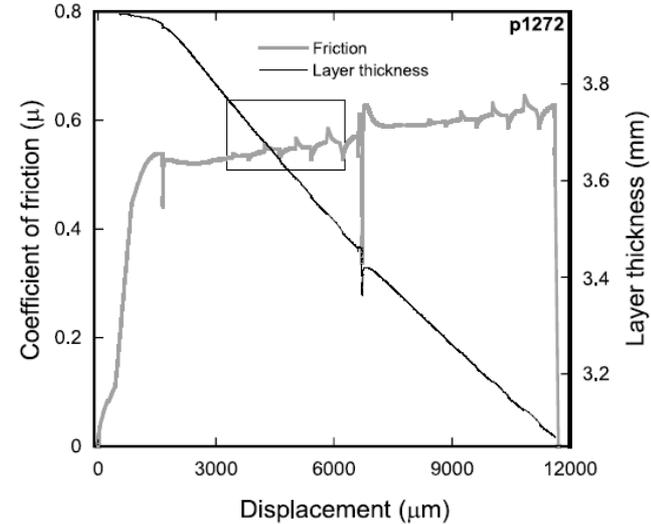


Rate-State Friction [1]

Velocity Steps



Multiple Velocity Steps



R-S Friction

$$\left. \begin{aligned} \mu &= \mu_0 + a \ln\left(\frac{v}{v_0}\right) + b \ln\left(\frac{v_0 \theta}{D_C}\right) \\ \frac{d\theta}{dt} &= 1 - \frac{v\theta}{D_C} \quad (\text{Dieterich Evolution}) \\ \frac{d\theta}{dt} &= \frac{-v\theta}{D_C} \ln\left(\frac{v\theta}{D_C}\right) \quad (\text{Ruina Evolution}) \end{aligned} \right\}$$

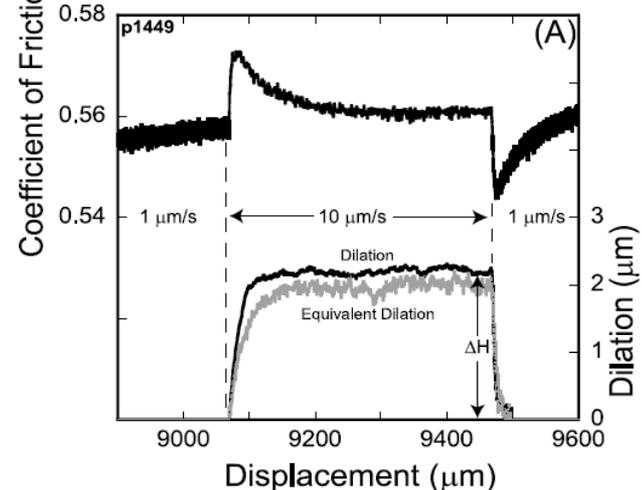
Dilation

$$\frac{\Delta H}{H} \cong \Delta \phi = -\epsilon \ln\left(\frac{v}{v_0}\right) = -\epsilon \ln\left(\frac{v_0 \theta}{D_c}\right)$$

Permeability Evolution

$$\frac{k}{k_0} = \left(1 + \frac{\Delta b}{b_0}\right)^3 = \left(1 + \frac{\Delta H}{H}\right)^3$$

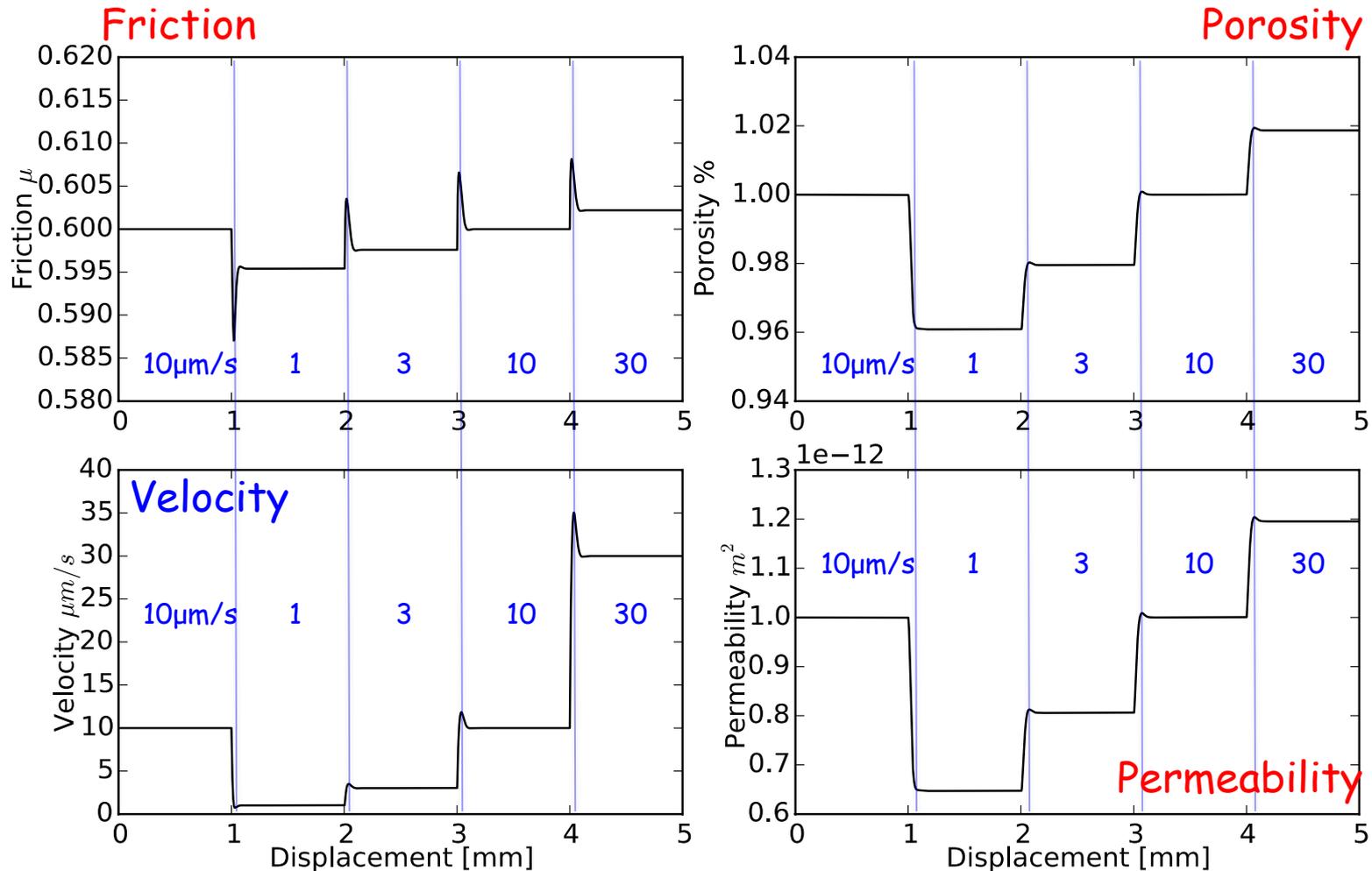
Single Velocity Step



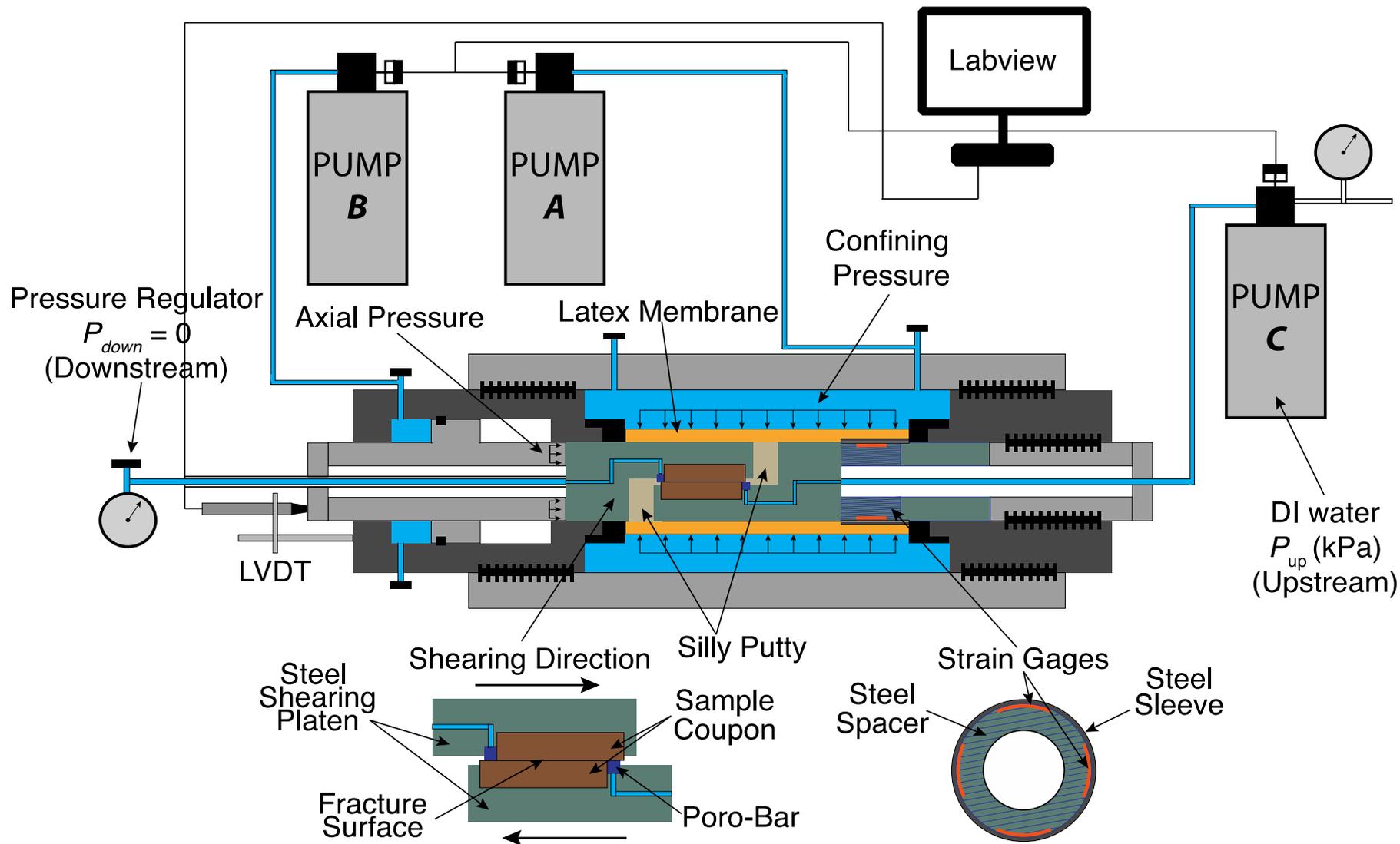
Rational Linkages: Rate-State Friction, Porosity and Permeability

$$\dot{\phi}_{plastic} = -\frac{V}{D_c}(\phi_{plastic} - \phi_{ss}), \quad \phi_{ss} = \phi_0 + \varepsilon \ln\left(\frac{V}{V_0}\right), \quad \frac{k(\phi)}{k_0} = \left(\frac{\phi - \phi_c}{\phi_0 - \phi_c}\right)^n$$

High Stiffness, positive dilatational coefficient

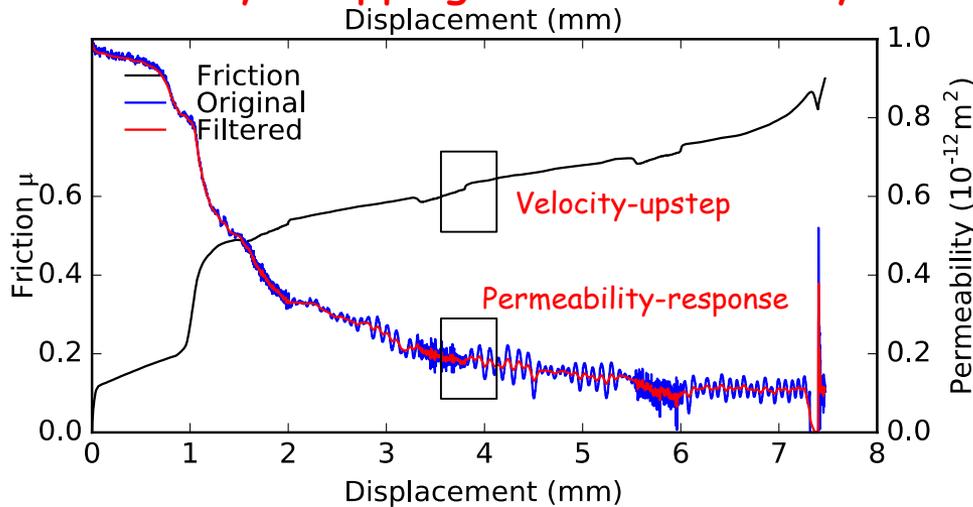


Frictional Stability-Permeability Experiments

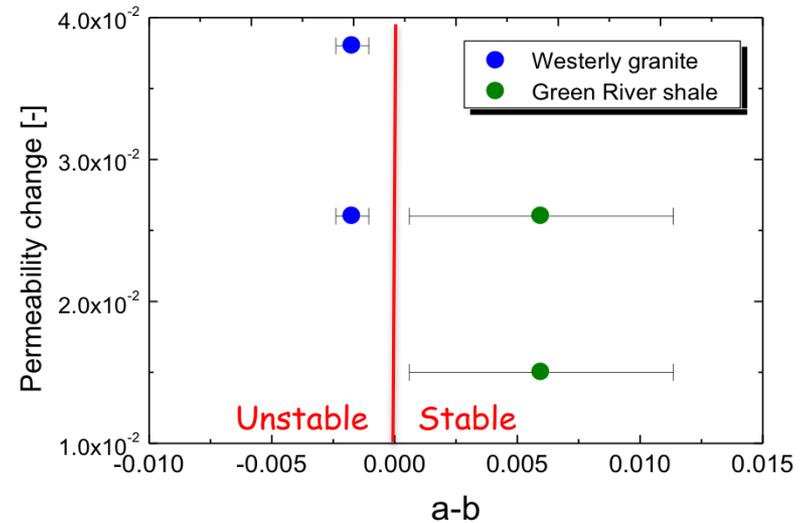


Frictional Stability-Permeability Observations

Velocity-stepping and Permeability

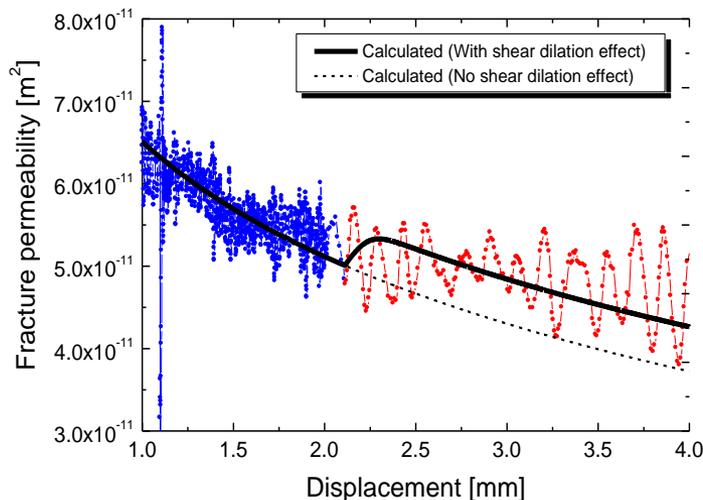


Permeability-Frictional Stability

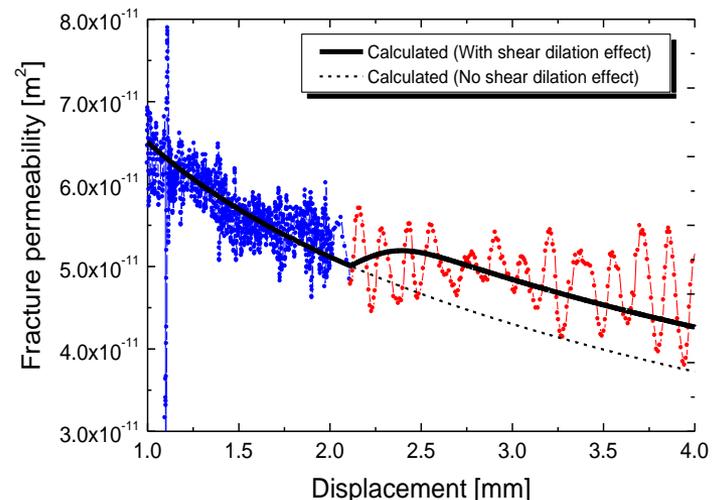


Permeability Evolution

$\varepsilon=0.0224$ ($n=2$), $D_c=50$ [μm]

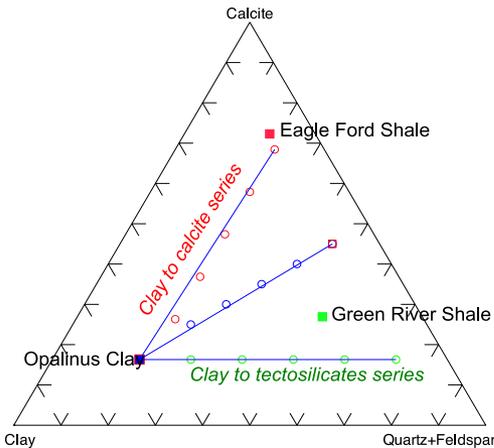


$\varepsilon=0.0224$ ($n=2$), $D_c=100$ [μm]

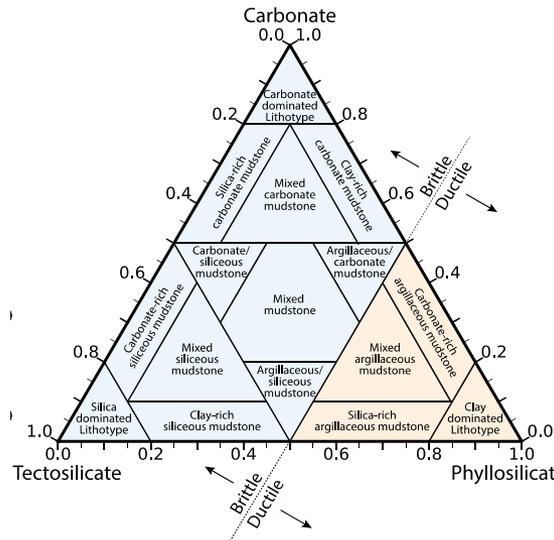


Mineralogical Sample Space

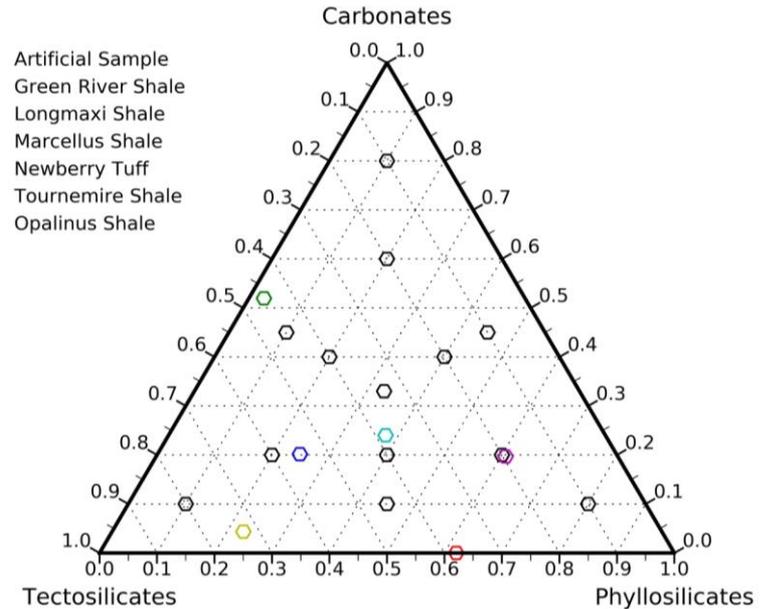
Sample Space for Artificial Samples:



Frictional Stability:

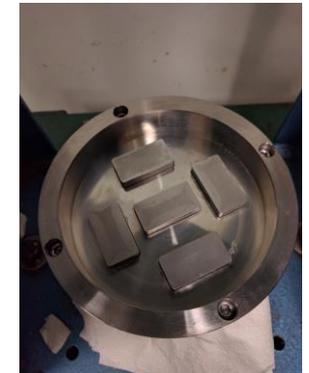
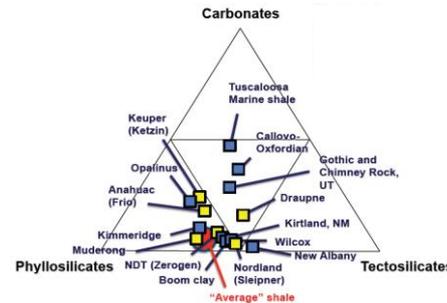


- Artificial Sample
- Green River Shale
- Longmaxi Shale
- Marcellus Shale
- Newberry Tuff
- Tournemire Shale
- Opalinus Shale



Natural Samples:

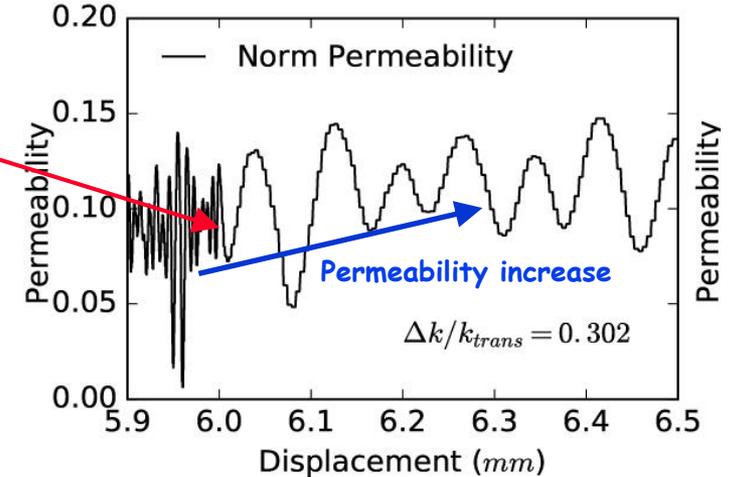
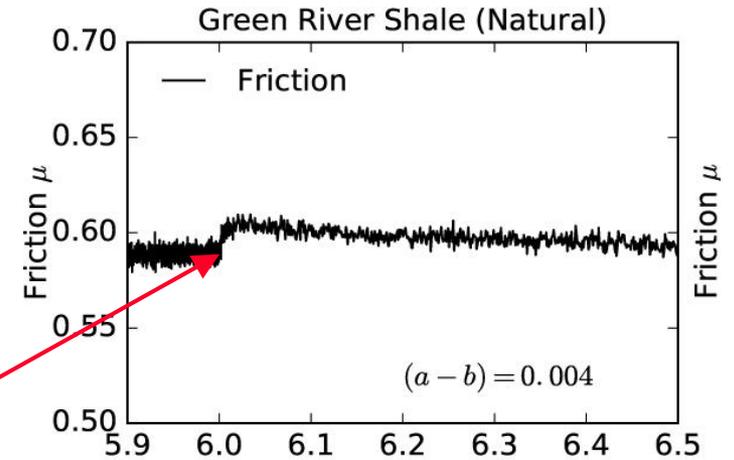
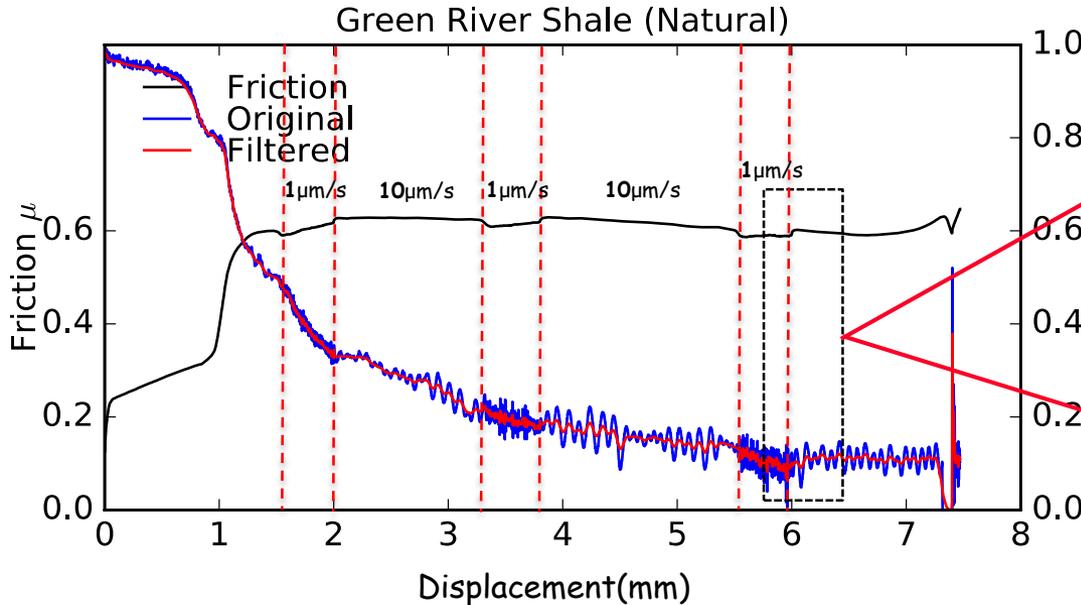
- (1) Green River Shale (Colorado, USA);
- (2) Longmaxi Shale (Chongqing, China);
- (3) Marcellus Shale (Pennsylvania, USA);
- (4) Newberry Tuff (Oregon, USA);
- (5) Tournemire Shale (France);
- (6) Opalinus Shale (Switzerland)



Bulk mineralogy of caprock formations
(Ian Bourg LBNL NCGC)

Green River Shale - Permeability Enhancement

	Tectosilicate	Carbonate	Phyllosilicate
Green River Shale	45.44%	51.96%	2.60%



Before

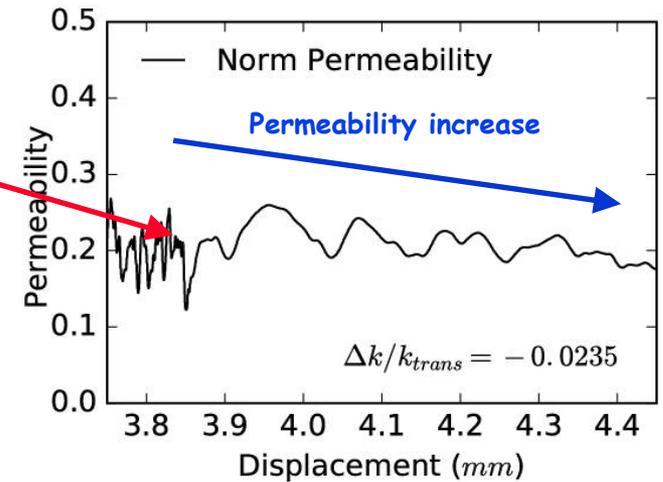
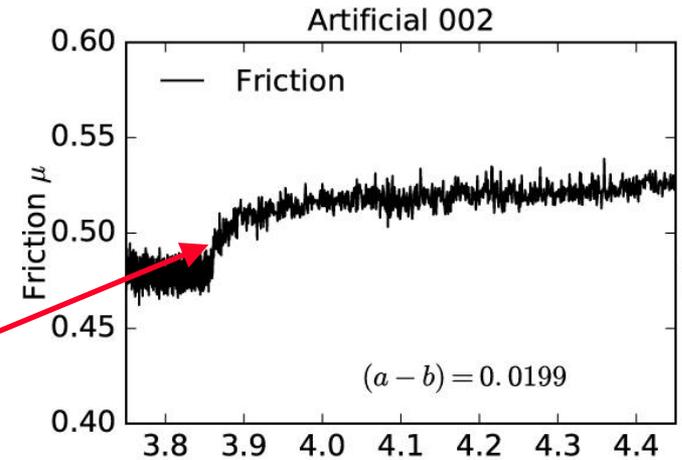
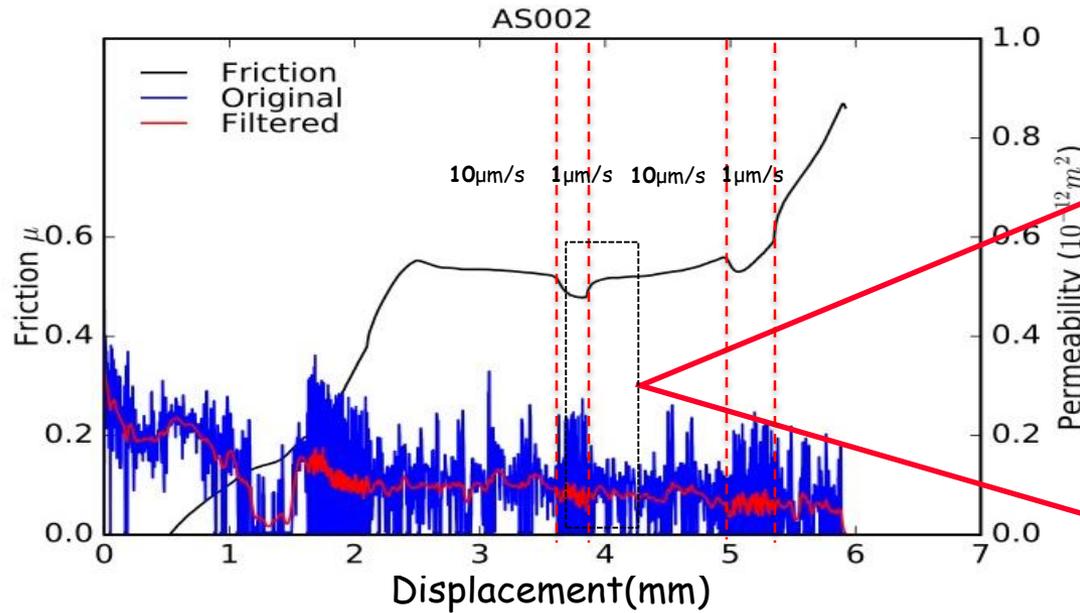
After

Wear products after slip

Velocity-upstep results in a permeability increase due to dilation

Phyllosilicate-dominant Artificial Sample - Permeability Decrease

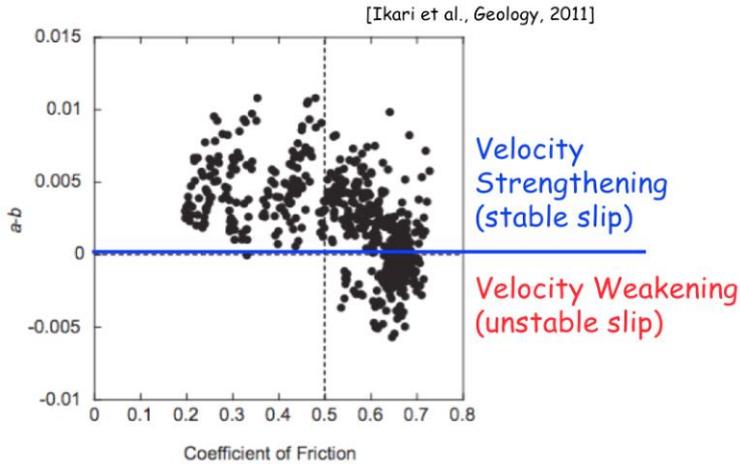
	Tectosilicate	Carbonate	Phyllosilicate
AS002	10%	10%	80%



Before After
Clay swelling concurrent
with shear damage

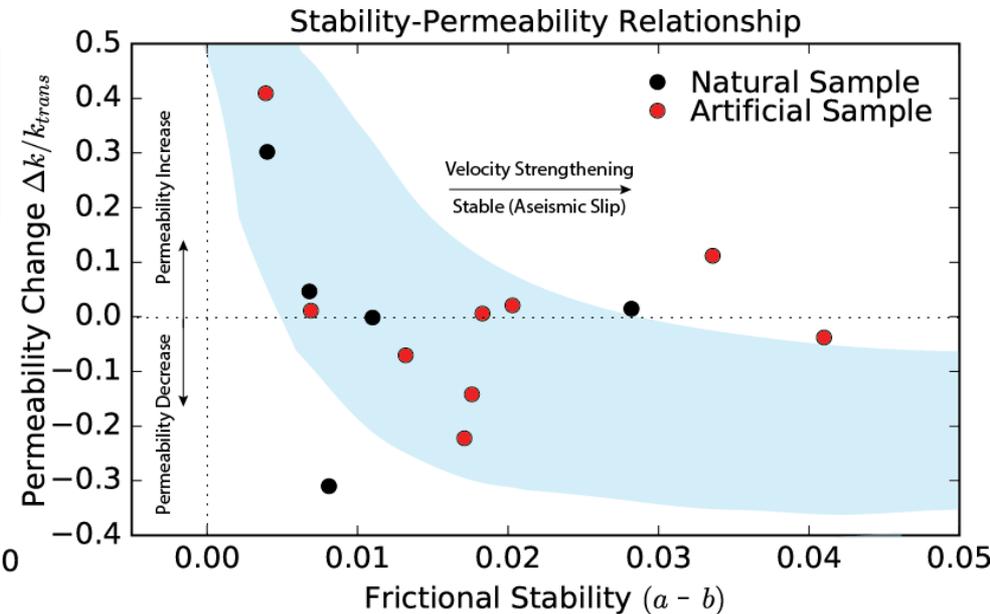
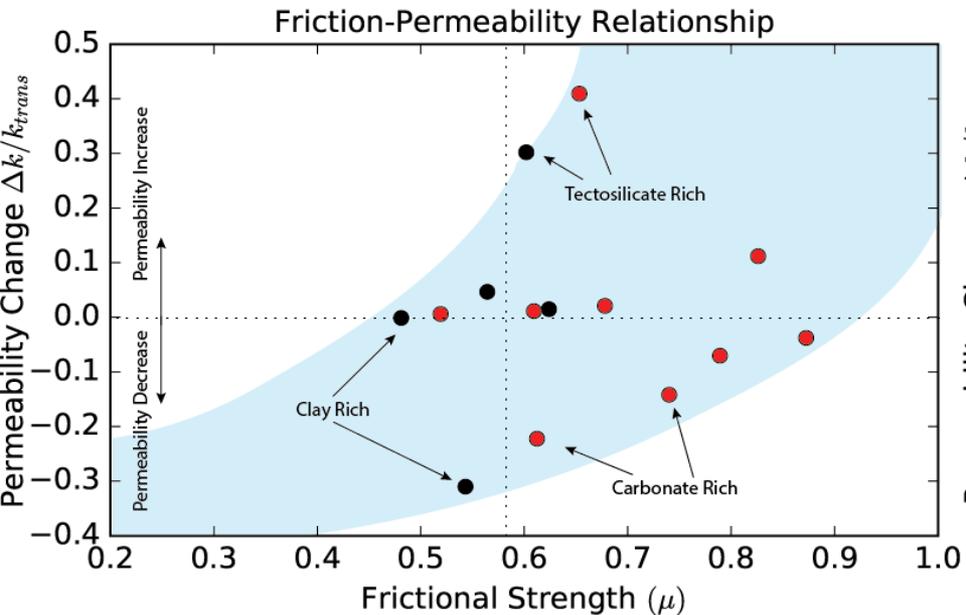
Velocity-upstep results in a permeability decrease due to wear products and swelling

Nascent Friction-Stability-Permeability Relationships



Observations

- dk/k_0 increases with increased brittleness $(a-b) < 0$
- dk/k_0 increases with increased frictional strength
- Roles of mineralogy and surface roughness?



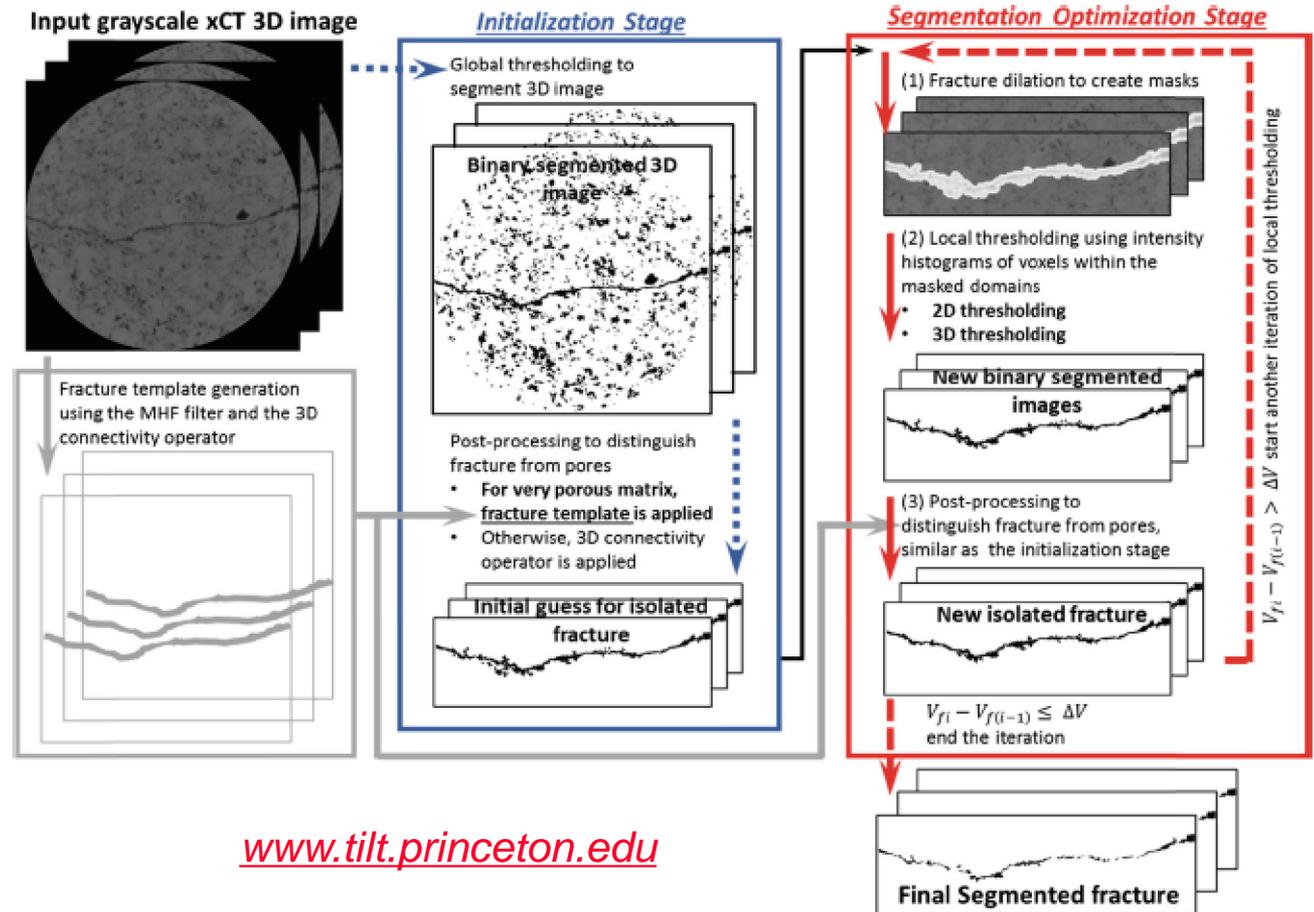
Quantifying fracture geometry with X-ray tomography

Post flow/shear subcores for xCT



xCT imaging at APS Sector 13 GSECARS

Developed 3D image segmentation method for complex fractures
'TILT' - for fractures with rough porous surfaces & wear products

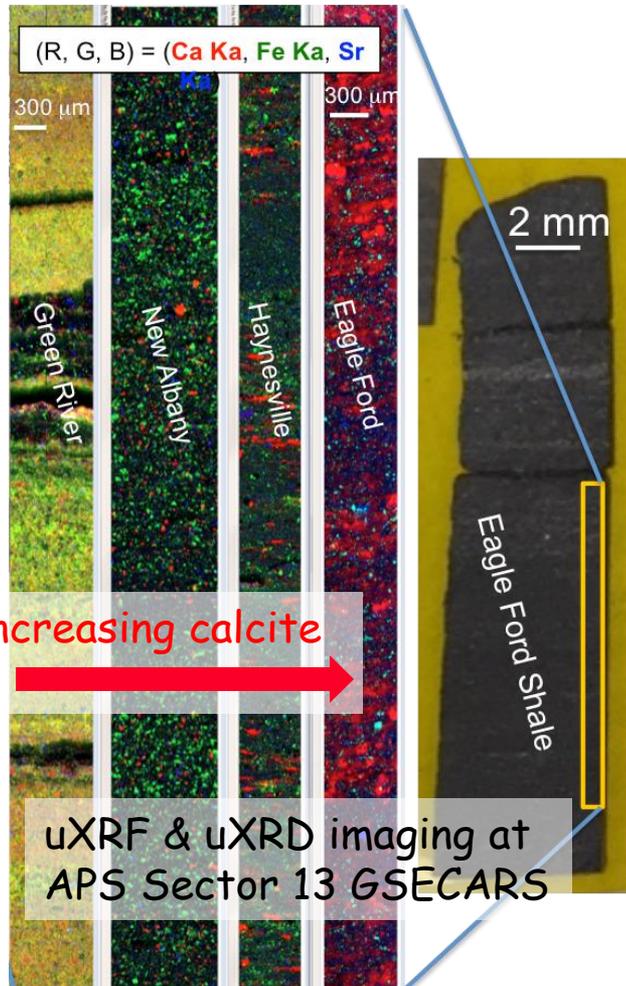


www.tilt.princeton.edu

Deng, H., Fitts, J.P. & Peters, C.A. *Comput Geosci* (2016) 20: 231.

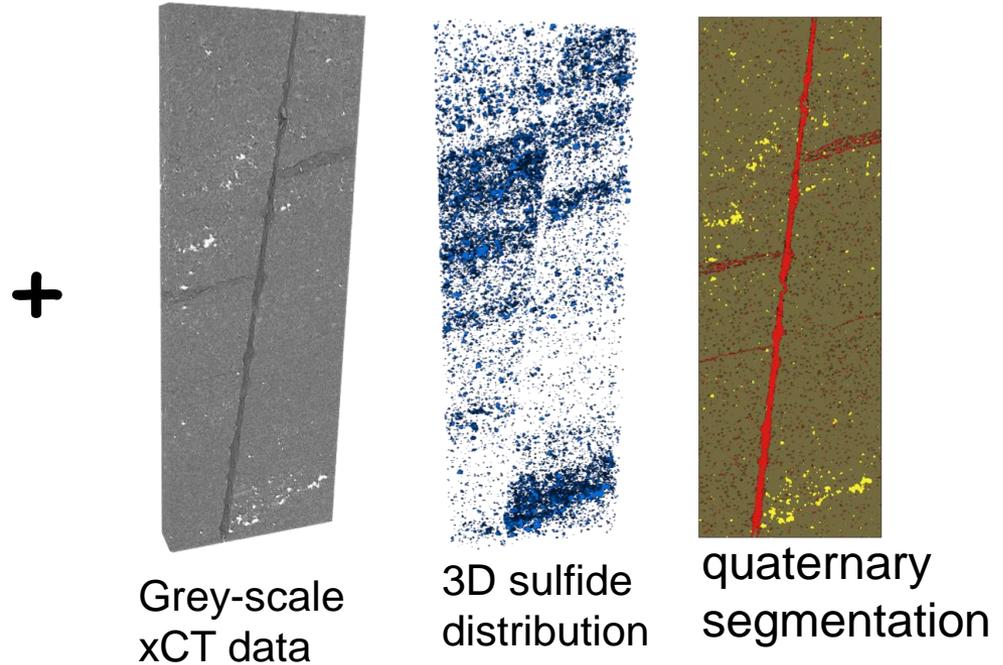
'Digital fractures' combine 3D xCT and fracture surface characterizations

2D fracture surface characterization
Detailed mineral spatial distribution and textures



3D xCT characterization

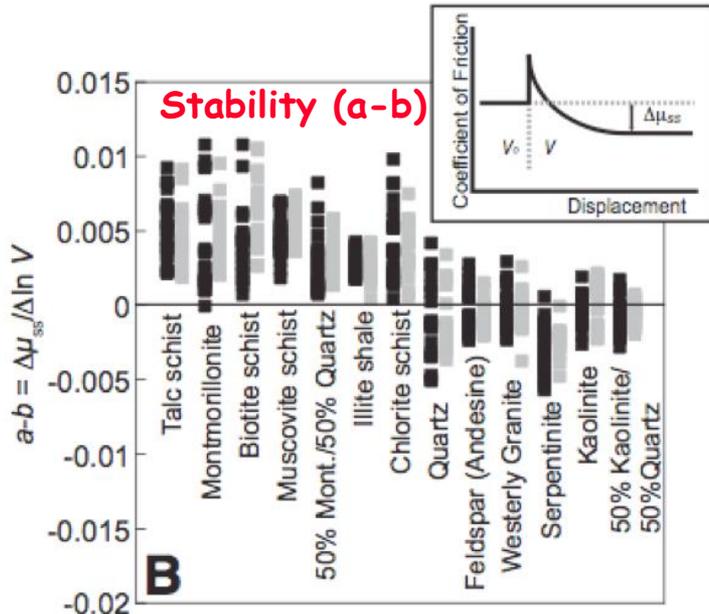
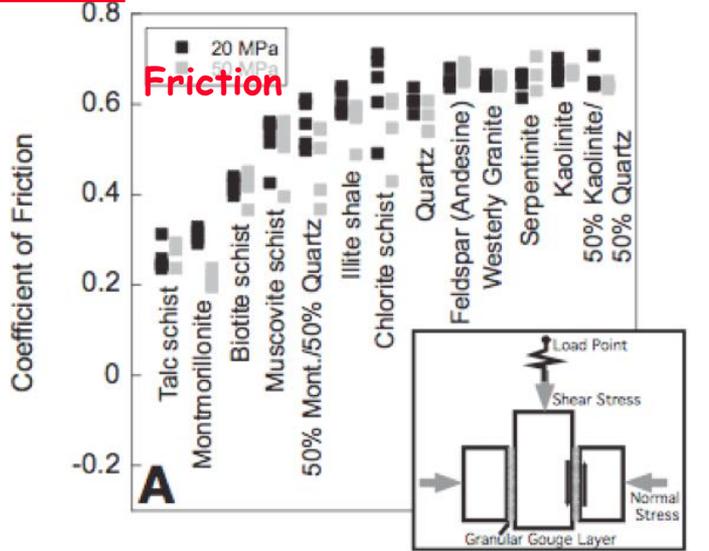
Aperture geometry, contacting asperities & coarse mineral distributions



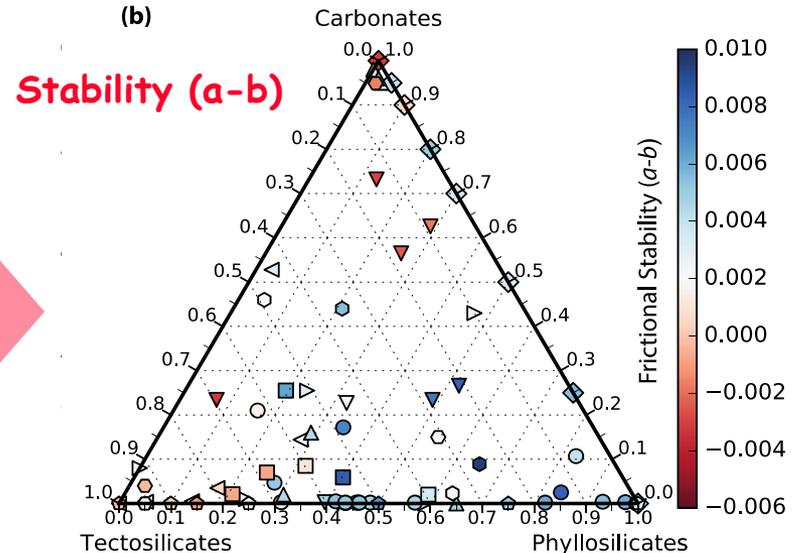
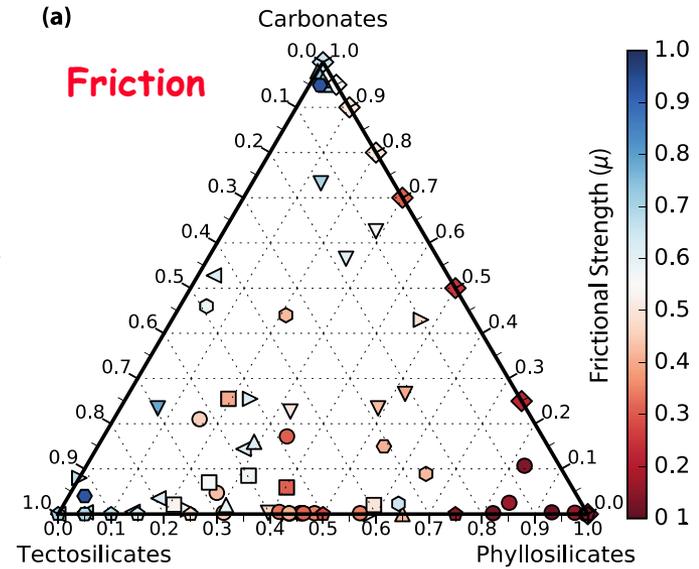
Inputs for simulating friction-stability-permeability evolution & deriving constitutive relations

Stability-Permeability Relations in Composites/Mixtures

Mono-mineralic

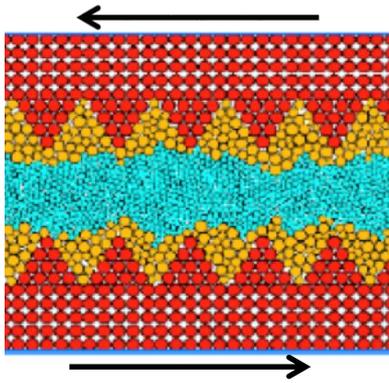


Multi-mineralic

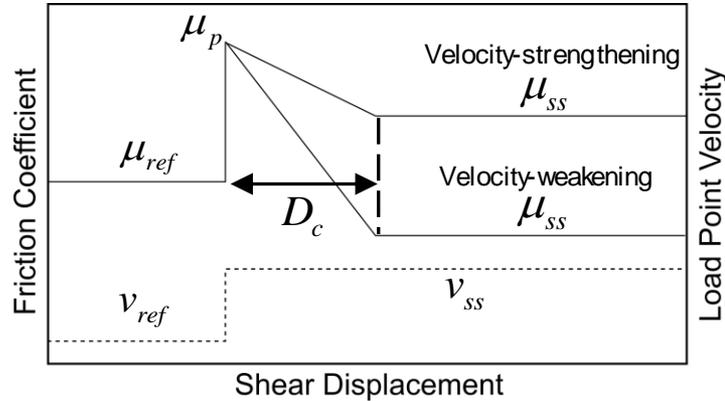


Multi-Mineral Frictional Strength

DEM Model



Particle-Particle Frictional



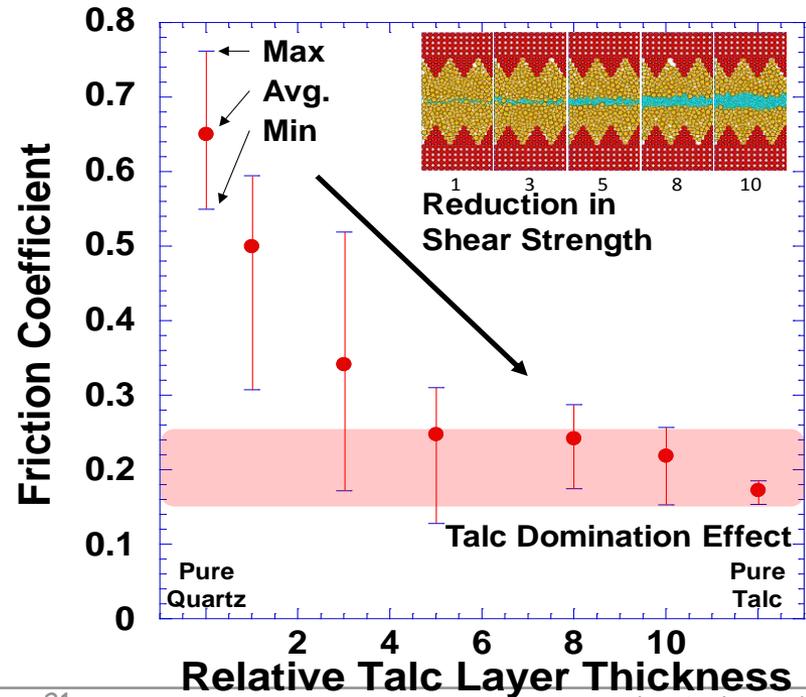
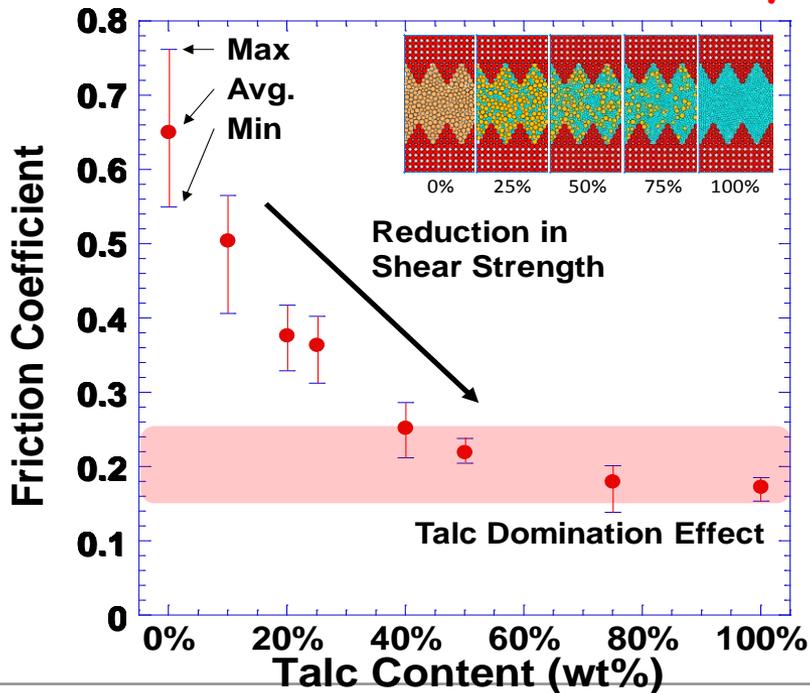
RSF Notation

$$\mu_p = \mu_{ref} + a \ln \left(\frac{V_{ss}}{V_{ref}} \right)$$

$$\mu_{ss} = \mu_{ref} + (a-b) \ln \left(\frac{V_{ss}}{V_{ref}} \right)$$

$$\mu = \begin{cases} \mu_p & D_{acc} = 0 \\ \mu_p - \left(\frac{\mu_p - \mu_{ss}}{D_c} \right) D_{acc} & D_{acc} \in (0, D_c) \\ \mu_{ss} & D_{acc} = D_c \end{cases}$$

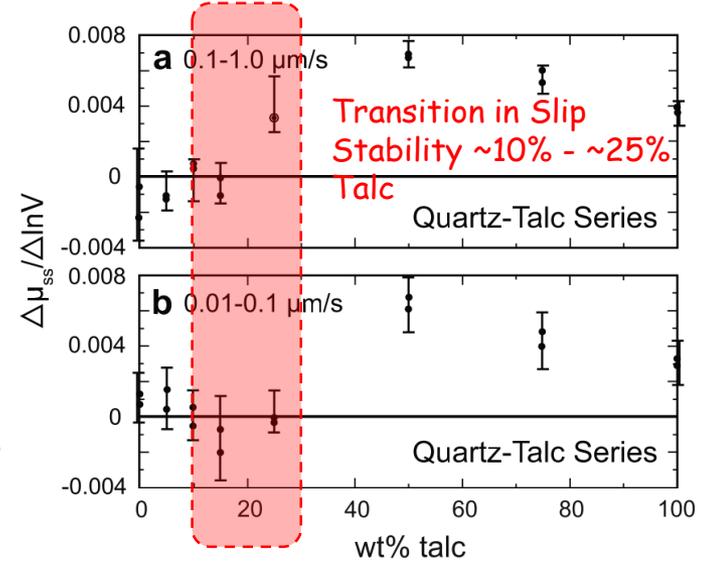
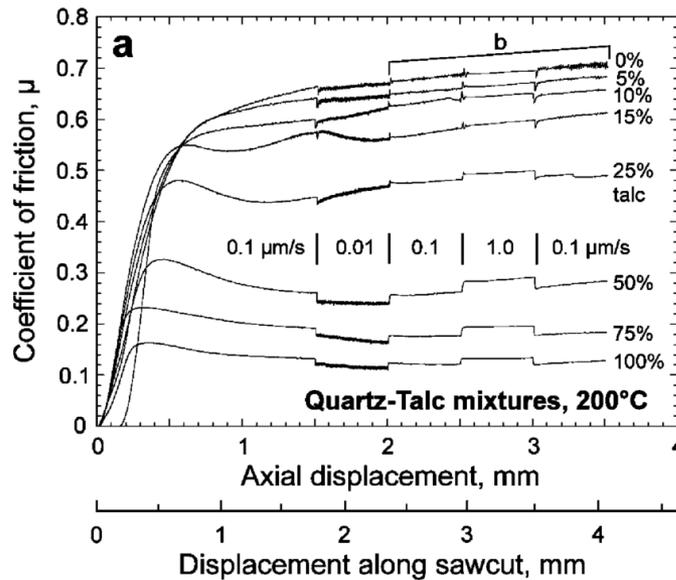
Steady-State Friction



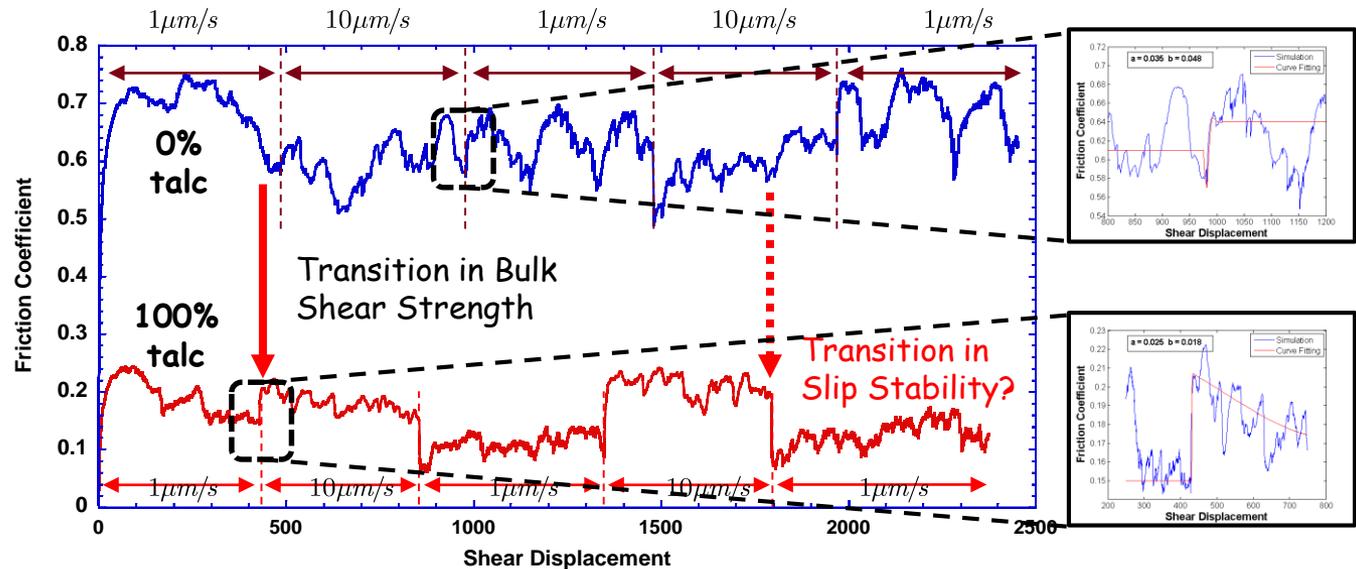
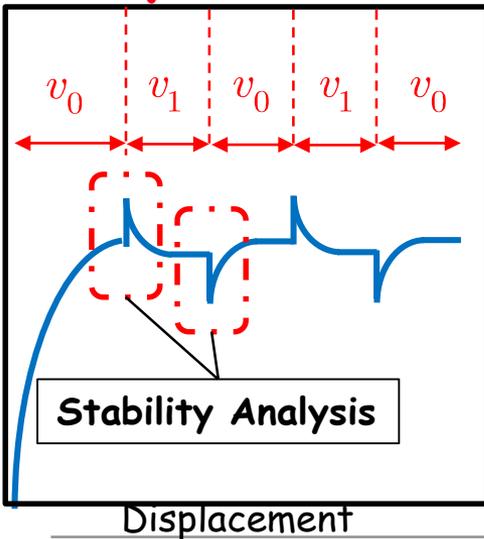
Mixture Controls of Frictional Instability

Observations

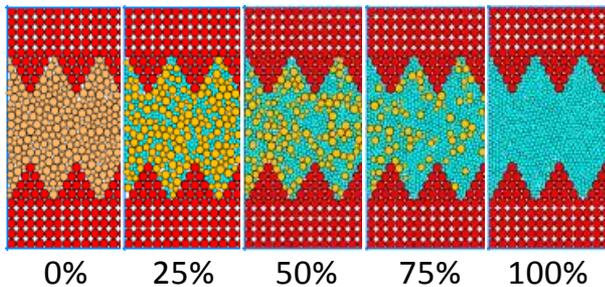
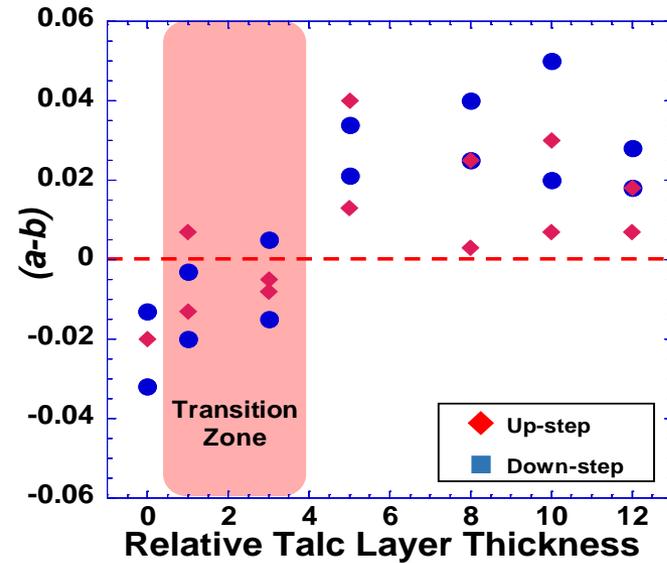
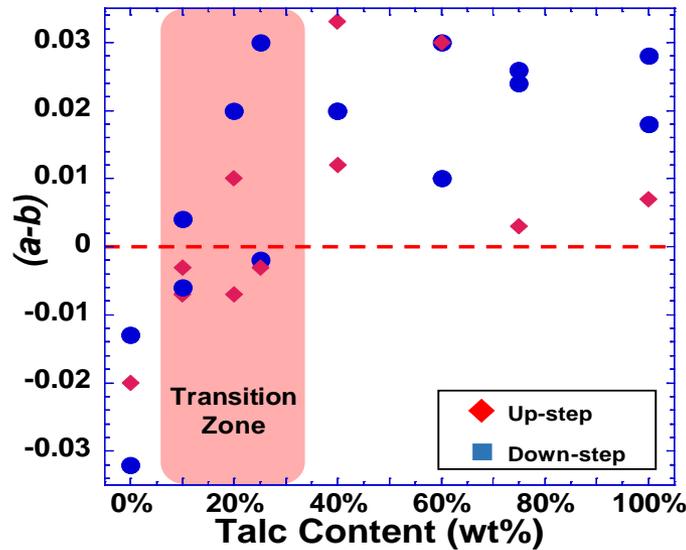
[Moore & Lockner 2011]



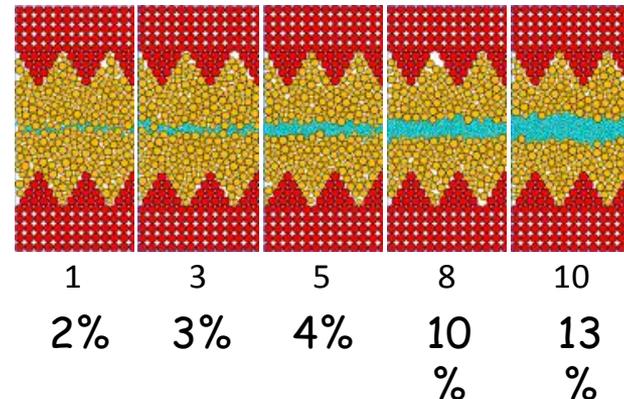
Analysis



Multi-Mineral Frictional Stability

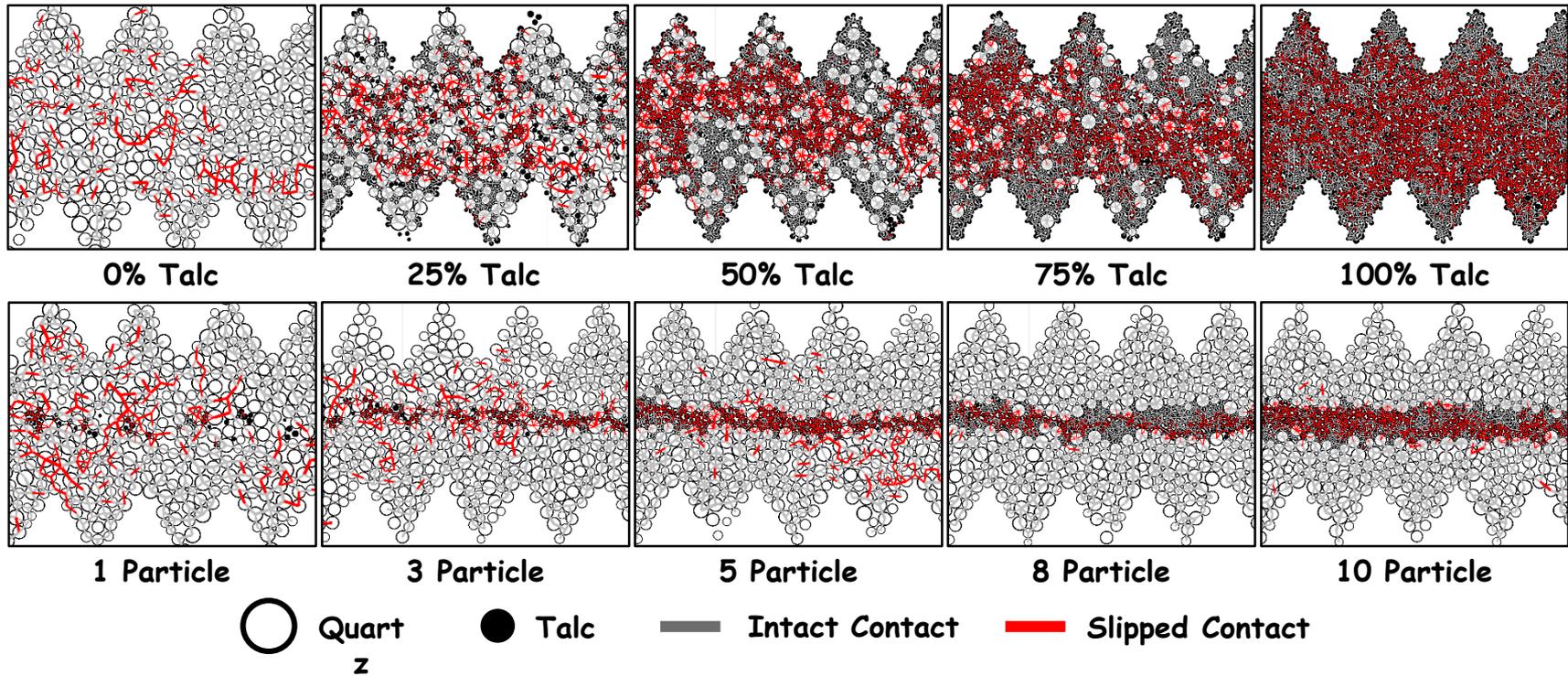


Transition zone appears at ~10% to ~25% talc content



Transition zone appears at ~2% to ~3% talc content

Texture-dependent Localization Effects



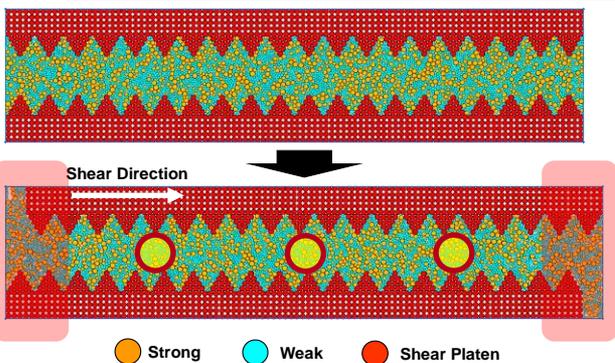
Distributed heterogeneity:

Slipped contacts are distributed homogeneously in the sample, following critical shear band directions.

Textured/layered:

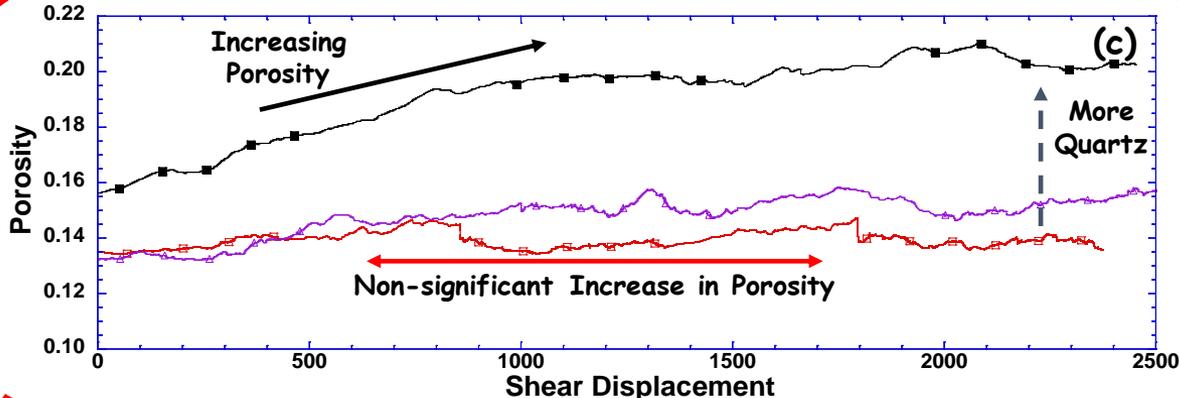
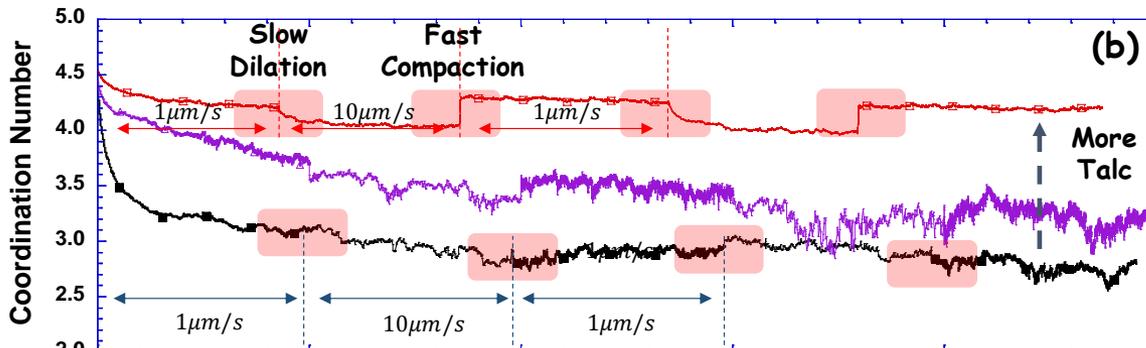
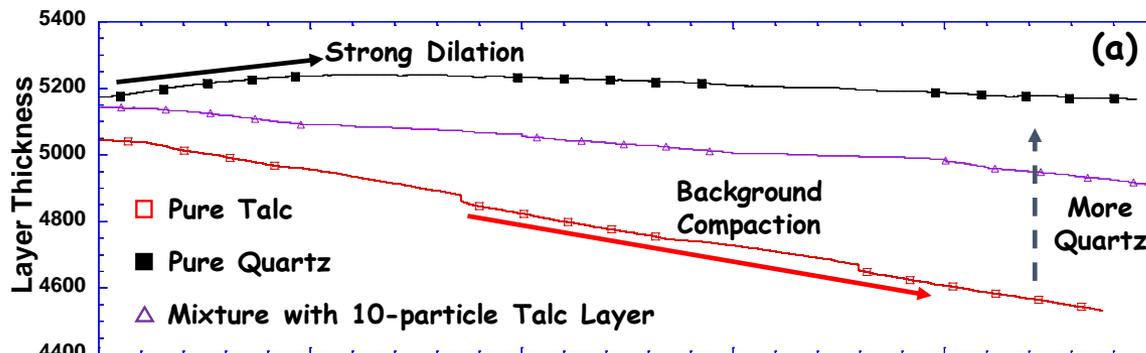
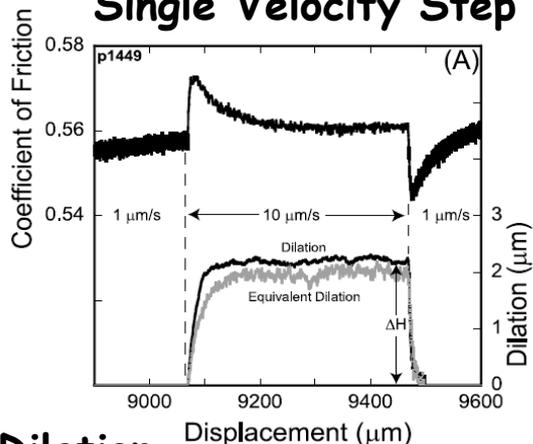
Slipped contacts are distributed inside talc/weak layer, forming a localized shear zone, forcing most slip to evolve within this zone.

Evolution of Layer thickness, Coord. Num, and Porosity



Background Compaction

Single Velocity Step



Dilatation

$$\frac{\Delta H}{H} \cong \Delta \phi = -\epsilon \ln\left(\frac{v}{v_0}\right) = -\epsilon \ln\left(\frac{v_0 \theta}{D_c}\right)$$

Permeability Evolution

$$\frac{k}{k_0} = \left(1 + \frac{\Delta b}{b_0}\right)^3 = \left(1 + \frac{\Delta H}{H}\right)^3 \cong (1 + \Delta \phi)^3$$

Coupling Reactive Transport and Mechanical Deformation

Research Questions & Methods

- For fractures in carbonate rocks exposed to acidified brine, how does the coupling of geochemical and geomechanical processes affect the pattern of dissolution and the subsequent evolution of fracture transmissivity?
- How does mineral heterogeneity impact the evolution of fracture geometry and transmissivity?
 - Keeping constant initial fracture geometry, pressure gradient, and inlet chemistry.

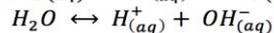
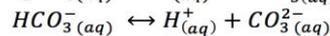
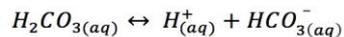
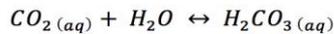
Approach: 2D Fracture Flow Model with Coupled Reactive Transport and Mechanical Deformation

2D Carbonate Reactive Transport Model

1. Transport

$$\frac{\partial}{\partial x} \left[b^3(x,y) \frac{\partial h(x,y)}{\partial x} \right] + \frac{\partial}{\partial y} \left[b^3(x,y) \frac{\partial h(x,y)}{\partial y} \right] = 0$$

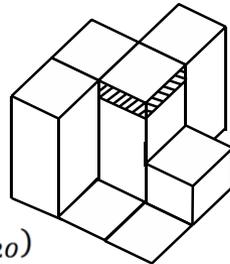
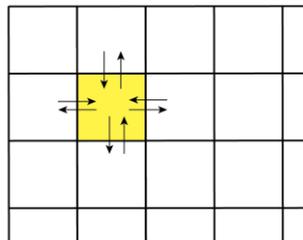
1. Speciation



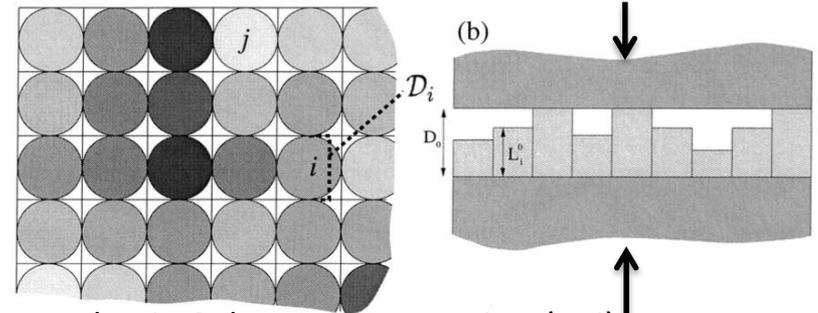
1. Reaction

$$R = A * k_f * \left(1 - \frac{IAP}{Ksp} \right)$$

$$k_f = k_1(a_{\text{H}^+}) + k_2(a_{\text{H}_2\text{CO}_3}) + k_3(a_{\text{H}_2\text{O}})$$



Mechanical Deformation Model



1. Elastic Column Compression (ΔL_i)

$$\Delta L_i = f_i \frac{L_i^0}{E\pi a^2}$$

1. Elastic half-wall deformation (W_i)

$$W_i = f_i * \frac{8(1-\nu^2)}{\pi^2 E a} I_4(a) + f_j * \frac{8(1-\nu^2)}{\pi^2 E a} I_3(r_{ij}, a)$$

Pyrak-Nolte & Morris, 2000

Initial Mineralogy

Aperture Change after 40 Hrs of Reaction

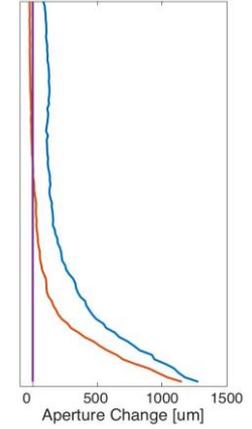
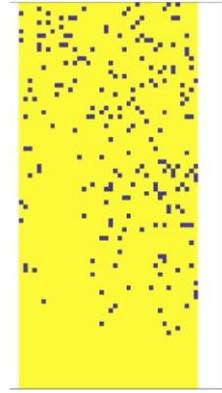
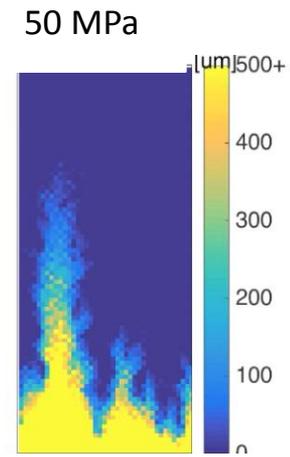
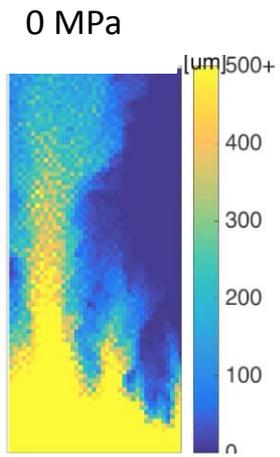
Contact Points

Aperture Change Vertical Profile

100% Pure Limestone



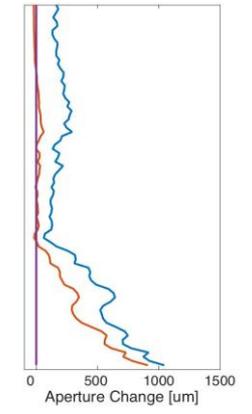
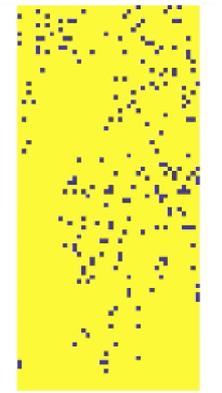
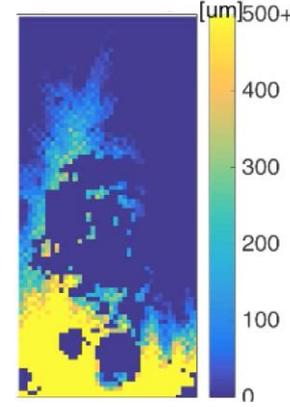
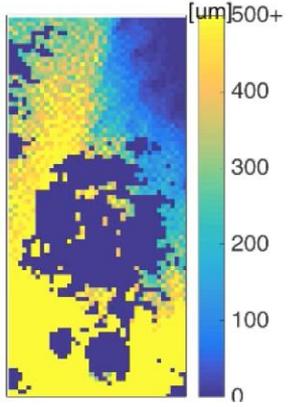
Direction of Flow ↑



Amherstburg Limestone



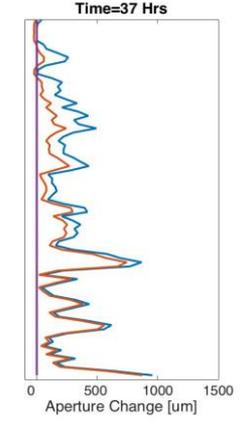
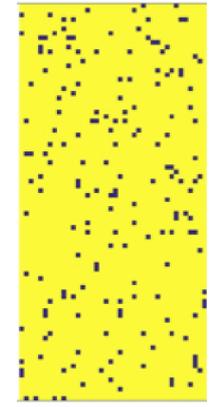
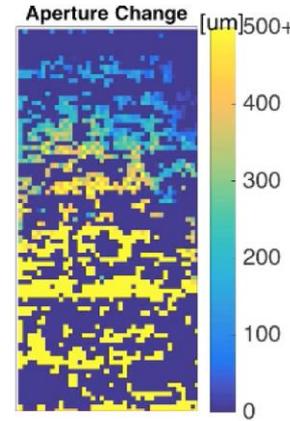
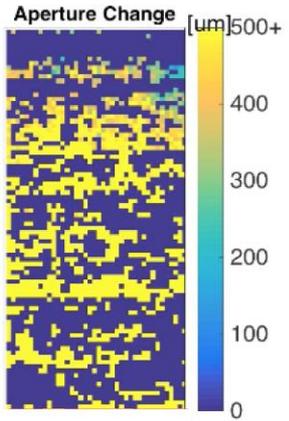
Direction of Flow ↑



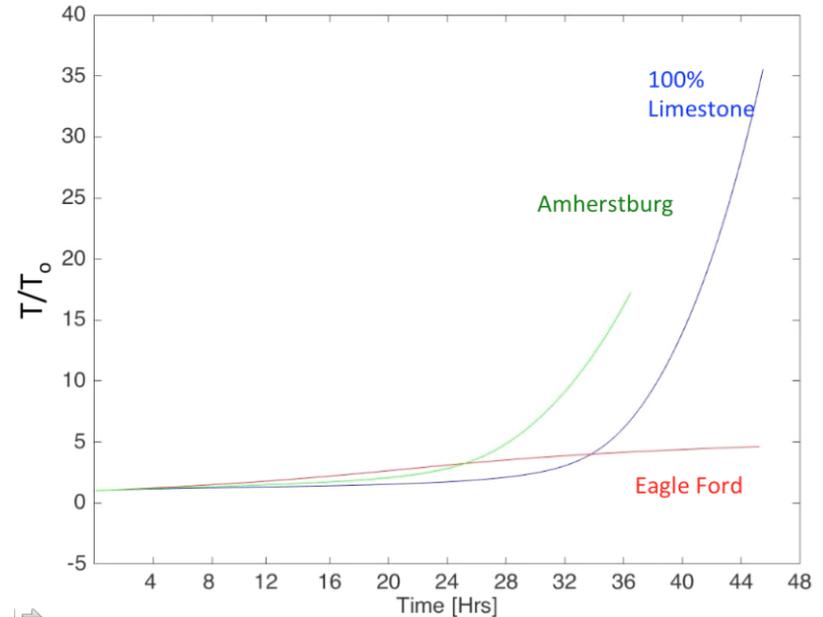
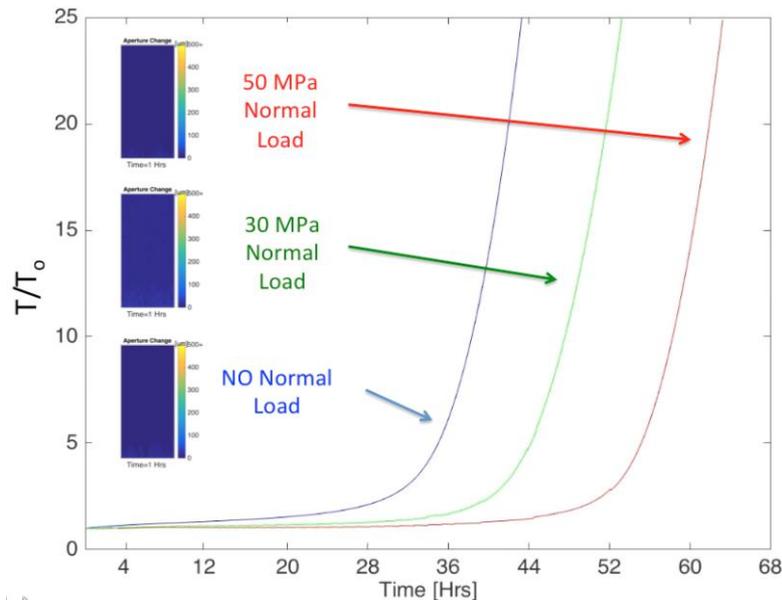
Eagle Ford Shale



Direction of Flow ↑



Transmissivity Change over Time



- When the rock is spatially homogenous mineralogically, transmissivity remains controlled by unreacted downstream apertures
 - When the rock includes areas of nonreactive minerals, the reactive front penetrates farther downstream faster, however certain mineral distributions can also inhibit channel formation
 - When mineral dissolution is combined with constant normal mechanical load, fracture closure delays transmissivity increase
-
- Future Projects:
 - Effect of reactive transport along fracture interfaces on fracture frictional properties

Accomplishments to Date

ACCOMPLISHMENTS

- Caprock Mineralogy
 - Broad range of samples acquired: Eagle Ford, Green River Shale and Opalinus....
 - Frictional strength of fabricated samples consistent with natural samples
- VS and SHS Experiments
 - Mechanisms-based seismicity-permeability evolution RSF-k
 - VS experiments on broad suite of natural and artificial samples
 - Nascent stability-permeability relations (indicate larger stability smaller dk)
- Imaging
 - Frozen post-test fractures
 - Completed first imaging and segmentation of sheared fractures
- Modeling
 - DRP models for friction and stability – gouge - compared with mixtures data
 - Enables testing of laboratory data for stability and permeability
 - Developed RT models for stiffness and permeability evolution of fractures

ONGOING

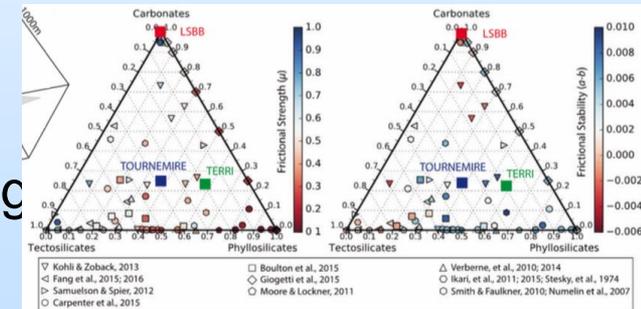
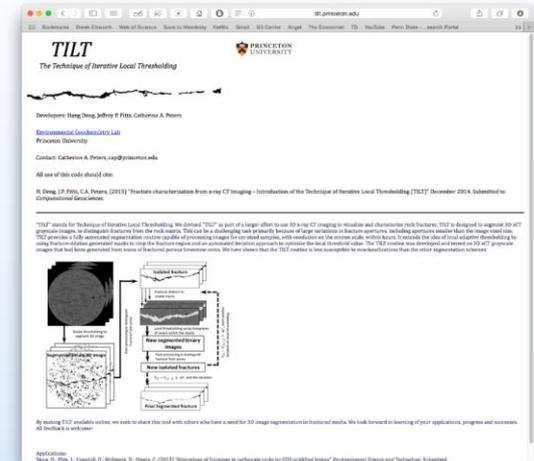
- Refine Mechanistic Understanding of Behaviors
 - VS stability experiments – systematic roles of mineralogy and additionally roughness
 - SHS experiments for healing and recurrence and consequences for multiphase flow
 - Reactive transport properties on sheared fractures
 - DRP models of Biot and transport properties
- Integrating modeling and experiments and imaging

Synergistic Opportunities

- TILT.princeton.edu

- Linkages with:

- Projects exploring petrophysical characterization as methods to deconvolve findings
- Projects exploring field scale response - URLs and field experimentation (Guglielmi, Aix-Marseille & LBNL)
 - Seismicity-permeability correlations
 - Linkages across scales for upscaling
 - LSBB (Carbonate), Tournemire (Shale), Mt Terri (Shale)
- Imaging *in vivo* (Dustin Crandall)



Summary

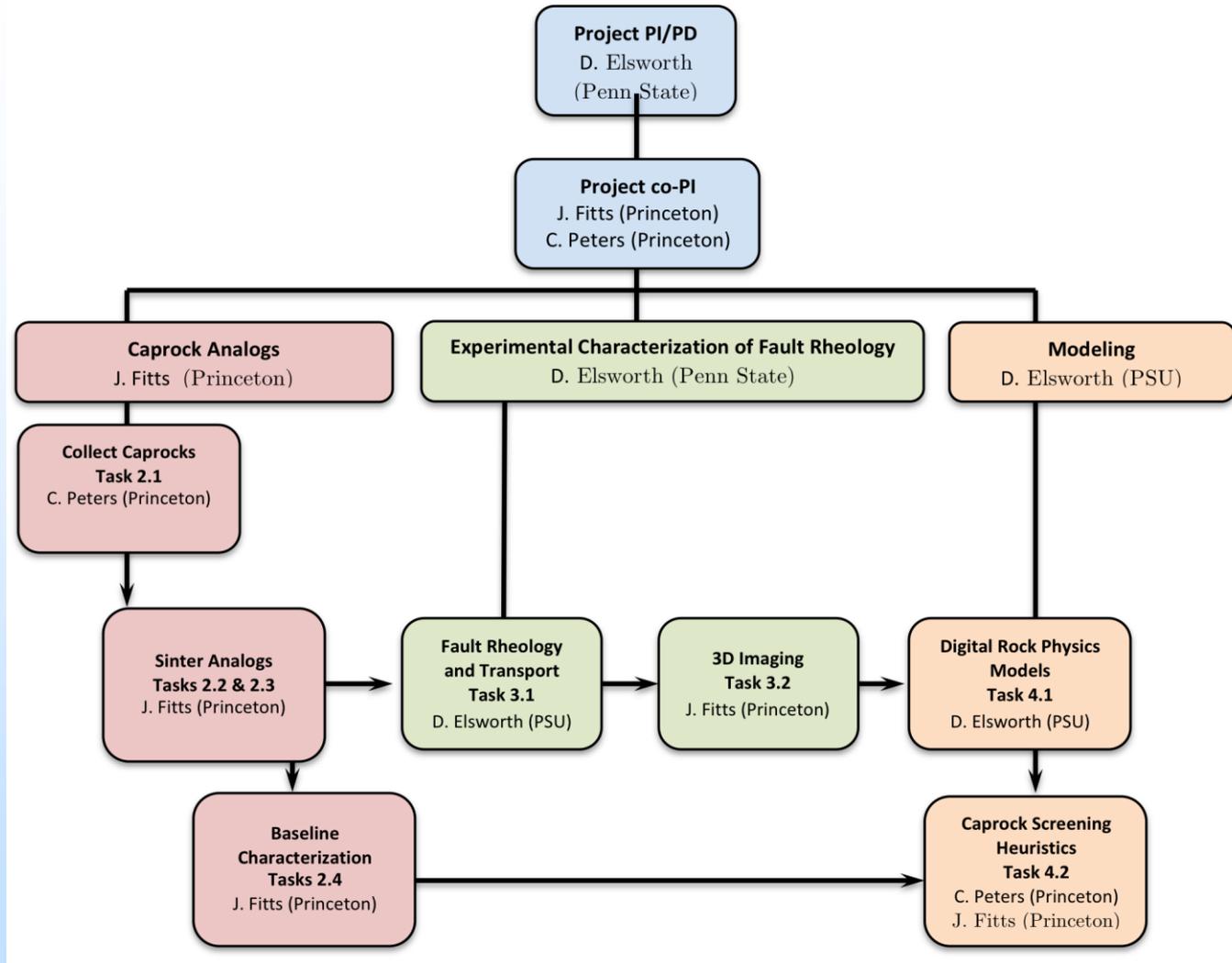
- Rupture of caprocks is a potentially important issue in CCS where:
 - Large overpressures may result from CO₂ injection
 - May result in seismic (felt) or aseismic rupture
 - May result in loss of inventory
- Absent and needed are data/information to constrain:
 - Seismic and aseismic reactivation of faults/fractures – distribution of felt/aseismic events?
 - Healing of faults/fractures – what are event recurrence intervals?
 - Evolution of multiphase flow and transport properties – likelihood of breaching and loss?
- Develop methodologies for:
 - Integration of process measurements and imaging at microscale
 - Scaling microscale-to-mesoscale via digital rock physics models as a new tool
- Apply to CCS by:
 - Enabling the screening of potential caprock materials for suitability and durability
 - Providing a consistent view of the likelihood and consequences of breached seals on seismic risk and loss of inventory for candidate CO₂ storage reservoirs.

Appendix Following

Appendix

Following

Organization Chart/ Communication Plan



Communication plan:

Biweekly Skype [Oct 23; Nov 6,]

Biannual meeting

Gantt Chart

SCHEDULE of TASKS and MILESTONES		BP1 Oct 2014 to Sept 2015				BP2 Oct 2015 to Sept 2016				BP3 Oct 2016 to Sept 2017																											
		Y1Q1	Y1Q2	Y1Q3	Y1Q4	Y2Q1	Y2Q2	Y2Q3	Y2Q4	Y3Q1	Y3Q2	Y3Q3	Y3Q4																								
		O	N	D	J	F	M	A	M	J	J	A	S	O	N	D	J	F	M	A	M	J	J	A	S	O	N	D	J	F	M	A	M	J	J	A	S
Task 1 -- Project management and planning	PI	[Task 1: Project management and planning - Active across all quarters]																																			
Task 2 -- Collect, synthesize and characterize sedimentary formation samples	Fitts	[Task 2: Collect, synthesize and characterize sedimentary formation samples - Active across all quarters]																																			
SubTask 2.1 -- Collect Homogeneous and Mineralogically Complex Sedimentary Rocks	Peters	[SubTask 2.1: Active in Y1Q1, Y1Q2, Y1Q3]																																			
SubTask 2.2 -- Sinter Mineral Mixtures to Create Idealized Analogs of Sedimentary Rocks	Fitts	[SubTask 2.2: Active in Y1Q2, Y1Q3, Y1Q4]																																			
SubTask 2.3 -- Conduct Baseline Characterization of Natural and Synthetic Caprocks (Fitts)	Fitts	[SubTask 2.3: Active in Y1Q2, Y1Q3, Y1Q4]																																			
Task 3 -- Laboratory Experimentation	Elsw orth	[Task 3: Laboratory Experimentation - Active across all quarters]																																			
Subtask 3.1 -- Evolution of Fault Rheology and Transport Parameters	Elsw orth	[Subtask 3.1: Active across all quarters]																																			
Subtask 3.2 -- 3D Imaging of fault contact area, fault geometry, and mineralogy & textures	Fitts	[Subtask 3.2: Active in Y1Q3, Y1Q4]																																			
Task 4 -- Modeling for Response and Caprock Screening	Elsw orth	[Task 4: Modeling for Response and Caprock Screening - Active across all quarters]																																			
Subtask 4.1 -- Digital rock physics of response	Elsw orth	[Subtask 4.1: Active across all quarters]																																			
Subtask 4.2 -- Caprock screening heuristics	Peters/Fitts	[Subtask 4.2: Active in Y1Q3, Y1Q4]																																			

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- Elsworth, D., Gan, Q., Fang, Y., Pogacnik, J., Taron, J., Izadi, G., Guglielmi, Y., Im, K.J., Wang, C., Ishibashi, T., Niemeijer, A., Candela, T. 2016. Induced seismicity and permeability evolution in EGS reservoirs – The good, the bad and the ugly. First Annual Darcy Center Symposium. *Mastering the Complexity of Fracture Networks*. Technical University of Eindhoven, Netherlands. June 2. [Keynote]
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- Spokas, K., Peters, C.A. (2016) Coupling Stress and Reactive Transport in Fractures: Effects of Mineralogy on the Evolution of Contacting Asperities and Fracture Permeability. XXI International Conference of Computational Methods in Water Resources. Toronto, Canada. June 20-24.
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